

Re: PER Drainage design review

(b) (4) [REDACTED]
[REDACTED]@gallupsurveyors.com>

Mon 11/11/2013 11:32 AM

To: (b) (4) [REDACTED]@eaest.com>;

Cc: Sturgeon, Randy <Sturgeon.Randy@epa.gov>; (b) (4) [REDACTED]@eaest.com>;
(b) (4) [REDACTED]@advantusstrategies.com (b) (4) [REDACTED]@advantusstrategies.com>; (b) (4) [REDACTED]@salmonsinc.com
(b) (4) [REDACTED]@salmonsinc.com>;

Categories: PER

1 attachments (3 MB)

PER DITCH STUDY.pdf;

Gentlemen,

See my response to comment 4 below, along with the attachments. Please call or write me if you have any questions.

Thanks-

David Butler

----- Original Message -----

From: (b) (4) [REDACTED]
To: (b) (4) [REDACTED]@gallupsurveyors.com
Cc: Sturgeon, Randy (Sturgeon.Randy@epa.gov) ; (b) (4) [REDACTED]
(b) (4) [REDACTED]@advantusstrategies.com> (b) (4) [REDACTED]@advantusstrategies.com) ; (b) (4) [REDACTED]
(b) (4) [REDACTED]@salmonsinc.com
Sent: Wednesday, October 23, 2013 1:55 PM
Subject: PER Drainage design review

(b) (4) [REDACTED]

EA has reviewed the latest drainage design and calculations for the PER property sent to EA on October 22. EA concurs with the submitted calculations and approach to manage the 100-year runoff from the 3975 Elm Avenue property. However, the pre- versus post-development ponding conditions have still not been quantified along the 3975 Elm Avenue/PER property line to show improvements to drainage conditions (see #4 below). The storm drain plan view layout has not changed since the last submittal but the storm drain pipe sizes have been increased and the pipe inverts have generally been lowered to decrease the water surface elevations in the system during the 100-year rainfall event. Additionally, a TideFlex valve has been added to the outfall of the storm drain system which conveys water from the 3975 Elm Avenue property. The following are EA comments provided to you on October 2 (in black) followed by EA's observations of the revised October 22 submission in red:

1. The times of concentration for runoff to reach each inlet appear high. This would affect the rainfall intensity, design flow rates, and performance of the system. Please confirm that 20-25 minutes is appropriate for the small drainage areas, especially since much of the area contains impervious surfaces.

The times of concentration have been revised and are appropriate for the drainage area size and land use. Additionally, the runoff coefficients (indicating imperviousness) have been revised to assume the 3975 Elm Avenue property will be fully developed in the future. Previous comment has been satisfied.

2. There appears to be a problem with the hydraulic grade line (HGL) calculations. Many of the computed HGLs are below the pipe inverts (Inlets 7, 6A, 4, 3, 2, 1, and 1A). This may be due to the friction slope used in the HGL calculations which are significantly different from the pipe slopes.

The hydraulic grade line calculations have been revised. The HGLs downstream of the 3975 Elm Avenue property are well below the proposed ground elevation of the PER improvements. HGLs along the 3975 Elm Avenue/PER property boundary are discussed in detail below.

3. Once the HGLs are corrected, it will be important to check the HGL at each manhole/flushed end section (FES) along the PER/3975 Elm Avenue property line to make sure water is not ponding along the proposed retaining wall. As a suggestion, it appears that the storm drain could be lowered to accommodate total capture of runoff from the 3975 Elm Avenue property with no backup. See attached "property line" pdf for concept. Please provide similar cross sections at critical points along the retaining wall for review (especially at STMH-4). Mr. (b) (6) is concerned with additional flow/velocity along the 3975 Elm Avenue property undercutting the existing concrete pad on his property. A cross section with HGL shown (similar to the attached pdf) may ease those concerns.

The HGL at each manhole/FES along the 3975 Elm Avenue/PER property line are contained within the existing ditch. There are 5 FESs along the property line that collect runoff from the 3975 property ranging in size from 12 inches to 36 inches. Water will pond in the ditch while the storm drain is flowing full during the 100-year storm event up to 1 foot as runoff enters the FESs.

4. Pete met with Mr. (b) (6) on 9/24 to discuss drainage patterns of the 3975 Elm Avenue property. Attached is an annotated C2 sheet indicating the drainage patterns on the property as described by Mr. (b) (6) and as confirmed during the visit. EA strongly suggests using similar drainage area delineations to the attached annotations to demonstrate to Mr. (b) (6) that his concerns have been addressed. Also, Mr. (b) (6) is very concerned about the capacity of the ditch between the PER property and his, and he is also very concerned about maintaining positive drainage from this area in the pipe along the swale alignment you are proposing. EA strongly suggests that you perform a pre-development conditions analysis to demonstrate that the proposed PER development will improve the drainage along the PER/3975 Elm Avenue property boundary in the post-development condition. This could be demonstrated through improved water surface elevations and lack of ponding in the ditch between the two properties.

The drainage areas have been revised per EA recommendations and recommended flow patterns have been accounted for. There is ponding in the ditch of up to one foot while runoff enters the storm drain system. Although the system has been designed to collect runoff and convey flows to the outfall effectively, without any significant ponding, it is unknown how this compares to the pre-development condition water surface elevations in the ditch as a pre-development analysis was not performed for comparison. EA still strongly suggests showing a calculation for the pre-development condition runoff and corresponding depth in the property line ditch for comparison to the post-development condition. It is anticipated that a simple flow rate calculation for the 3975 Elm Avenue property and a cross section calculation using Manning's equation would be sufficient to show the pre-development flow depth in the ditch. Additionally, EA recommends adding check dams immediately downstream of each lateral inlet/FES into the main pipeline along the PER/3975 Elm Avenue property boundary to more effectively collect and drain the runoff from the ditch and to reduce the potential of bypass.

Check dams have been added just downstream of flared end sections at structures 1, 1A, 2, and 3. See plan sheets C4 and C5 and detail shown on sheet C7. Calculations for pre and post ponding elevations for two cross sections, A-A and B-B are provided on three 8.2 x 11 sheets. Conclusions on the bottom of sheets 2 and 3 show a lower water surface elevation in the ditch, post developed situation. The ditch in a pre developed state does not have adequate capacity for most of its length. The ditch, altered with the addition of a retaining wall, has capacity and 100 year flows are contained. The reason for the radical difference in pre and post states is most of the water that outfalls to the ditch from the (b) (6) side is intercepted by a new flared end section and piped in an storm sewer independent of the PER storm sewer. Additional, some of the overland flows from the PER site are eliminated in the post development state. See 2 attached drainage area maps. The (b) (6) water is piped and outfalls in the upper reaches of the current ditch and because of lack of slope and the general geometry of the trapazoidal ditch, it does not have capacity for the design storm in its existing predeveloped state. If and when the (b) (6) tract is developed, PER will have provided a storm sewer to accommodate 100 year (quantity, not quality) flows from the (b) (6) site.

Please let Jason Coleman or myself know if you have any further questions.

Pete Pellissier

PRE DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 1 OF 3
11/9/13

CHECK WATER SURFACE ELEVATION OF EXISTING DITCH BETWEEN PER AND DIXON: THE WATER SURFACE ELEVATION WILL BE CHECKED AT VARIOUS LOCATIONS ALONG THE RECENTLY CUT PERIMETER DITCH BASED ON FLOWS FROM A PRE DEVELOPMENT STAGE. THE DIXON PROPERTY HAD A DITCH IN THE SAME GENERAL LOCATION PRIOR TO PER PURCHASING THE PROPERTY AND THAT DITCH IS DEPICTED ON THE STEVE BOONE TOPOGRAPHIC SURVEY. SHORTLY AFTER PER PURCHASED AND CLEARED THE PROPERTY, A NEW TRAPAZOIDAL DITCH WAS CUT. THIS DRAINAGE ANALYSIS WILL ATTEMPT TO DETERMINE THE WATER SURFACE ELEVATION IN THE RECENTLY CUT TRAPAZOIDAL DITCH BASED ON A PRE DEVELOPMENT STATE.

PER PLANS ON INSTALLING A RETAINING WALL ON THE PER SIDE, 36" EAST OF THE COMMON BOUNDARY LINE. INSTALLING THE WALL WILL ALTER THE CROSS SECTIONAL GEOMETRY OF THE TRAPAZOIDAL DITCH. CALCULATIONS WILL BE PERFORMED TO DETERMINE THE WATER SURFACE ELEVATION OF THE ALTERED DITCH BASED ON POST DEVELOPMENT CONDITIONS.

SECTION A-A SHOWN ON PRE DEVELOPMENT DRAINAGE AREA MAP:

TOTAL DRAINAGE AREA: 135,343 S.F.=3.1070 ACRES
PERVIOUS AREA @ C FACTOR=0.2, 37,539 S.F.=0.8618 ACRES; CA=0.1724
PERVIOUS AREA @ C FACTOR=0.3, 42,388 S.F.=0.9731 ACRES; CA=0.2919
IMPERVIOUS AREA @ C FACTOR=0.9, 55,416 S.F.=1.2722 ACRES; CA=1.1450
SUM OF THE CA's=1.6093; C=0.5179

TIME OF CONCENTRATION:

200 L.F. OF OVERLAND FLOW @ 1.5% = 22.5 MINS

151 L.F. OF CHANNEL FLOW @ 1.5 FPS = 1.7 MINS

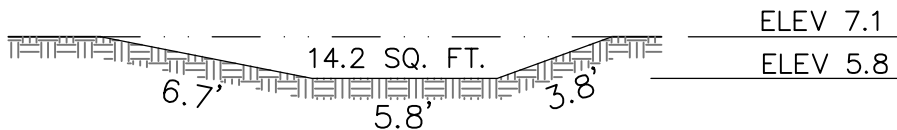
SUM T_c = 24.2 MINS

$I_{100} = 285.2/24.7+24.2 = 5.83$ IN/HR.

$I_{110} = 201/23.9+24.2 = 4.18$ IN/HR.

$Q_{100} = 1.6093 \times 5.83 = 9.4$ CFS

$Q_{110} = 1.6093 \times 4.18 = 6.7$ CFS



SECTION A-A

$WP = 6.7 + 5.8 + 3.8 = 16.3'$

$XS\ AREA = 14.2\ S.F.$

$R = A/WP = 14.2/16.3 = 0.87$

$N\ FACTOR\ FOR\ LINING = 0.45$

$SLOPE\ OF\ DITCH = 0.005\ FT/FT$

$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50}$ EQUALS DITCH CAPACITY
 $Q\ CAPACITY = 3.02 << 6.7\ OR\ 9.4\ CFS$

WATER SURFACE ELEVATION AT SECTION A-A IS 7.1 SINCE IT IS NOT CONTAINED WITHIN THE GEOMETRY OF THE DITCH SECTION.

POST DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 2 OF 3
11/9/13

NOTE:

END SECTION AT STMH-1 TAKES IN 1.93 ACRES FROM THE DIXON TRACT PIPE OUTFALLING AT THAT LOCATION. 1.93 ACRES WILL NO LONGER FLOW THROUGH THE DITCH, BUT WILL BE INTERCEPTED BY THE NEW PER STORM DRAIN AT STMH-1

AREAS DRAINING TO THE DITCH AT AND UPSTREAM OF SECTION A-A

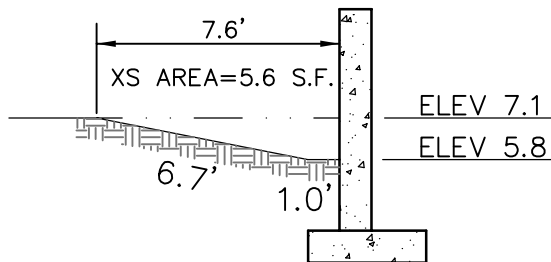
3199 S.F. = 0.0734 AC. X 0.5 = CA = 0.0367

1672 S.F. = 0.0384 AC X 0.5 = CA = 0.0192

SUM CA's: 0.0559

Tc=5 MINS, I100=28502/24.7+5 = 9.60 IN./HR.

Q100=0.0559 X 9.6 = 0.54 CFS



SECTION A-A

WP=6.7+1.0=7.7

XS AREA=5.6 S.F.

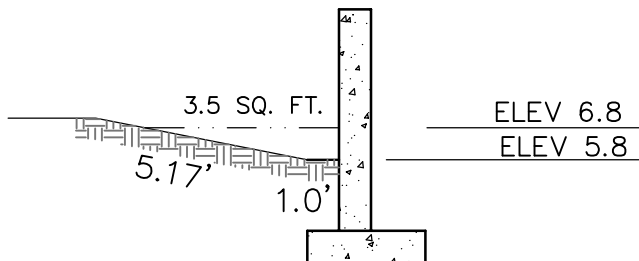
R=A/WP = 5.6/7.7 = 0.73

N FACTOR FOR LINING=0.45

SLOPE OF DITCH=0.005 FT/FT

$$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50} = 1.05 \text{ CFS AT FULL DEPTH OF 1.3'}$$

CAPACITY



WATER DEPTH OF WATER=12": (ELEV 6.80)

WP=5.17+1.0=6.17

XS AREA=3.54 S.F.

R=A/WP = 3.54/6.17 = 0.57

N FACTOR FOR LINING=0.45

SLOPE OF DITCH=0.005 FT/FT

HW ELEV. FROM PIPE CALCULATION
SHEET LD-269 SHOWS A HEADWATER
ELEV. OF 6.67

6.80 > 6.67; CONTROLLING ELEV=6.80

$$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50} = 0.56 \text{ CFS, APPROX. = TO 0.54 CFS}$$

CAPACITY

CONCLUSION:

THE 100 YEAR STORM ON A PRE DEVELOPED CONDITION IS NOT CONTAINED IN THE EX. DITCH SECTION AND WILL REACH A MIN. ELEVATION OF 7.1 (TOP OF DITCH BANK); SINCE WATER IS REMOVED FROM THE DITCH VIA ONSITE GRADING AND WITH THE ADDITION OF A FES AT STMH-1, THE WATER SURFACE PROFILE ELEVATION IS LOWER AT POST DEVELOPED CONDITIONS.

PRE DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 3 OF 3
11/9/13

AREAS:

3.107 AC. AT $C=0.5179$, $CA=1.6091$

1.2495 AC. AT $C=0.25$; $CA=0.3123$

SUM CA 's = 1.9214

TIME OF CONCENTRATION:

OVERLAND FLOW TIME=22.5 MINS

CHANNEL TIME. 626 L.F. @ 1.5 FPS=6.95 MINS

SUM T_c = 29.45 mins

$1100=285.2/24.7+29.45 = 5.26$ IN./HR.

$Q_{100}=1.9214 \times 5.26 = 10.1$ CFS

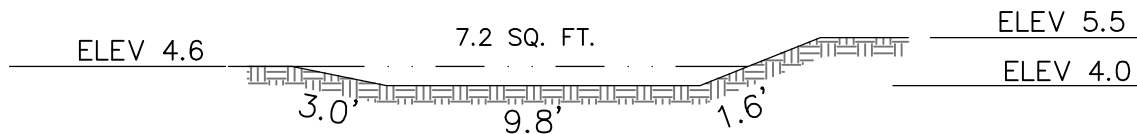
AVE DITCH SLOPE FROM XS A TO XS B: $5.9-4.7/475' = 0.0025$ FT/FT

XS AREA TO ELEV. 4.6 = 7.2 S.F.

$WP=3.0+9.8+1.6=14.4'$

$R=7.2/14.4=0.50$

N FACTOR FOR LINING=0.45

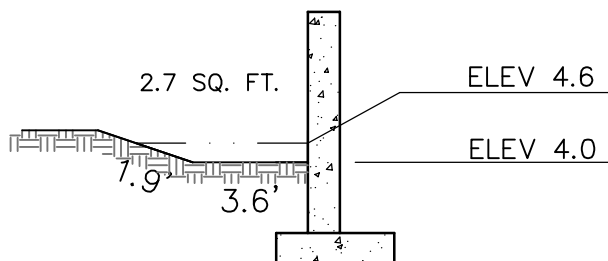


SECTION B-B

$Q=1.486/N \times A \times R^{0.67} \times S^{0.50}$ EQUALS DITCH CAPACITY
 Q CAPACITY=0.74<<10.1 CFS

DESIGN STORM ON A PRE DEVELOPED CONDITION
IS NOT CONTAINED IN THE DITCH GEOMETRY

POST DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH



SECTION B-B

AREA DRAINING TO XS-B:

1514 S.F.=0.0347 AC.

$C=0.50$

$CA=0.0173$

$T_c=5$ MINS, $1100=9.60$ IN/HR

$Q_{100}=0.17$ CFS

N FACTOR FOR LINING=0.45

AVG. DITCH SLOPE FROM XS A TO XS B: $5.9-4.7/475' = 0.0025$ FT/FT

XS AREA TO ELEV. 4.6 = 2.7 S.F.

$WP=1.9'+3.6'=5.5'$

$R=2.7/5.5=0.49$

$Q=1.486/N \times A \times R^{0.67} \times S^{0.50}$ EQUALS DITCH CAPACITY
 Q CAPACITY=0.28 CFS

CONCLUSION:

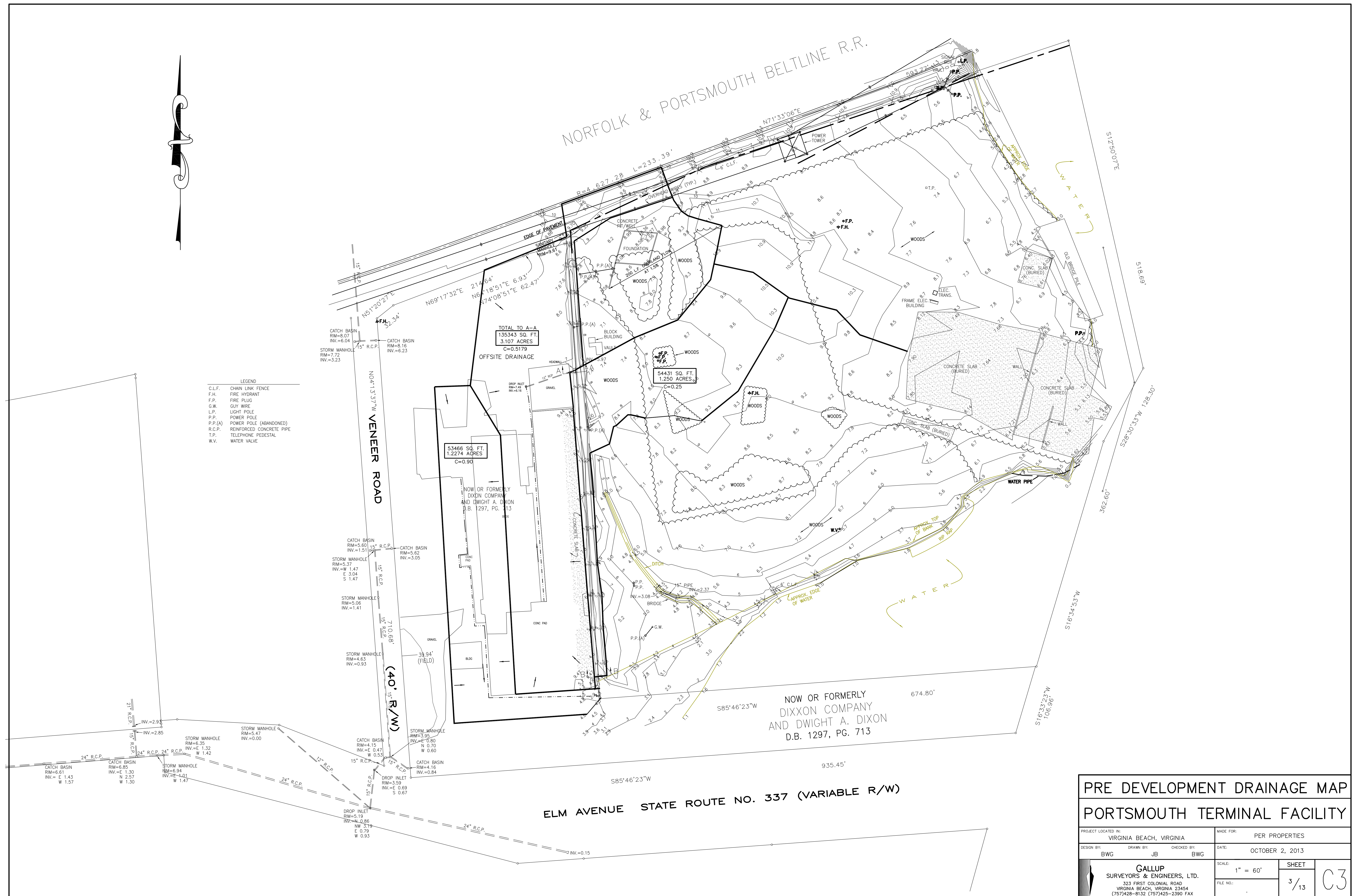
Q_{100} POST DEVELOPMENT=0.17 CFS

DITCH CAPACITY=0.28 CFS

WATER SURFACE ELEV. WILL BE LESS THAN TOP OF BANK ELEV OF 4.6

WATER SURFACE ELEV BEFORE DEVELOPMENT IS AT TOP OF BANK ELEV OF 4.6

SINCE THE STORM IS NOT CONTAINED.



DRAINAGE STRUCTURE SCHEDULE

1A. STMH RIM 10.50 INV 4.37	8. STMH RIM 10.50 INV -1.05	10-10A 208'-24" HDPE @ 0.25% INV IN 4.77, INV OUT 4.25
1. STMH RIM 10.50 INV 4.24	10. DI RIM 9.80 INV 4.77	10A-11 207'-24" HDPE @ 0.25% INV IN 4.25, INV OUT 3.73
2. STMH RIM 10.50 INV 4.04	11. DI RIM 9.80 INV 3.73	11-12 198'-24" HDPE @ 0.20% INV IN 3.73, INV OUT 3.33
3. STMH RIM 10.50 INV 3.73	12. STMH RIM 10.40 INV 3.33	12-12A 59'-24" HDPE @ 0.34% INV IN 3.33, INV OUT 3.13
4. STMH RIM 8.20 INV (N) 3.51 INV (E) -0.14 INV (W) 2.50	12A. DI RIM 9.50 INV 3.13	12A-13 191'-24" HDPE @ 0.34% INV IN 3.13, INV OUT 2.49
5. STMH RIM 10.20 INV -0.37	13. DI RIM 9.35 INV 2.49 (E,W,S) INV 7.29 (N)	RR-13 117'-12" HDPE @ 1.03% INV IN 8.50, INV OUT 7.29
6. DI RIM 9.40 INV (E) -0.58 INV (W) 1.87 INV (S) 3.41	14. DI RIM 9.35 INV 2.96	9A-8A 109'-18" PERFORATED HDPE @ 0.60% INV IN 4.09, INV OUT 3.44
7. STMH RIM 10.50 INV -0.86	15. DI RIM 9.35 INV 3.23	15-14 89'-18" HDPE @ 0.30% INV IN 3.23, INV OUT 2.96
5A. DI RIM 9.10 INV 5.09	7A. DI RIM 9.50 INV (N,S) 2.00 INV (E) 4.00	
10A. DI RIM 9.80 INV 4.25	8A. RIM 9.60 INV 3.44	
	9A. RIM 9.35 INV 4.09	
	6A. RIM 9.80 INV -0.57	

NOTES:
THE SILT SACK PRODUCT SHOWN ON SHEET C7 IS TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN PERMANENT FOR DRAINAGE STRUCTURES 7A, 8A, 9A, AND 13.

THE INVERTS SHOWN ON THE DROP INLET DENOTES THE INVERT OF THE PIPES. PROVIDE A 12" DEEP SUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS FOR MAINTENANCE PURPOSES FOR STRUCTURES 7A, 8A, 9A, AND 13.

O.W. DENOTES REQUIRED OBSERVATION WELLS; SEE DETAIL ON SHEET C9.

ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING. FINAL SURFACE WILL BE GRAVEL AND CRUSHED CONCRETE

PIPE SCHEDULE

4-5 150'-36" HDPE @ 0.15% INV IN -0.14, INV OUT -0.37	14-13 196'-24" HDPE @ 0.24% INV IN 2.96, INV OUT 2.49
5-6A 154'-36" HDPE @ 0.13% INV IN -0.37, INV OUT -0.57	13-7A 215'-18" PERFORATED HDPE @ 0.23% INV IN 2.49, INV OUT 2.00
6A-7 220'-36" HDPE @ 0.13% INV IN -0.57, INV OUT -0.86	7A-6 344'-36" CL. IV RCP @ 0.62% INV IN 4.00, INV OUT 1.87
7-8 158'-36" HDPE @ 0.12% INV IN -0.86, INV OUT -1.05	8A-7A 215'-24" CL. IV RCP @ 0.67% INV IN 3.44, INV OUT 2.00
8-OUTLET 152'-36" HDPE @ 0.12% INV IN -1.05, INV OUT -1.23 PROVIDE TIDEFLEX TF-1 ON OUTLET END	5A-6 330'-15" HDPE @ 0.51% INV IN 5.09, INV OUT 3.41
	6-OUTLET 144'-42" HDPE @ 0.50% INV IN -0.58, INV OUT -1.30 PROVIDE TIDEFLEX TF-1 ON OUTLET END

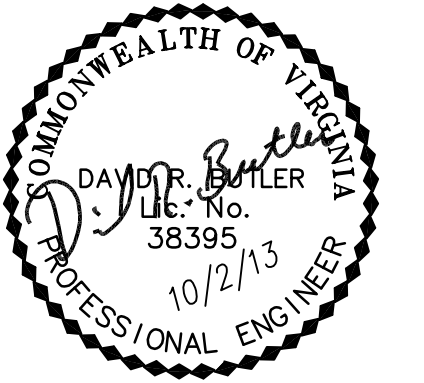
1A-1 134'-12" HDPE @ 0.10% INV IN 4.36, INV OUT 4.23	AT STMH-4: 6'-36" HDPE WITH 36" FES INV IN 2.85, INV OUT 2.50
1-2 119'-30" HDPE @ 0.17% INV IN 4.23, INV OUT 4.04	AT STMH-3: 10'-18" HDPE WITH 18" FES INV IN 4.80, INV OUT 3.73
2-3 204'-30" HDPE @ 0.15% INV IN 4.04, INV OUT 3.73	AT STMH-1A: 10'-12" HDPE WITH 12" FES INV IN 5.90, INV OUT 4.36
3-4 156'-30" HDPE @ 0.15% INV IN 3.73, INV OUT 3.50	AT STMH-1: 10'-30" HDPE WITH 30" FES INV IN 5.80, INV OUT 4.23
AT STMH-2: 10'-18" HDPE WITH 18" FES INV IN 5.50, INV OUT 4.04	

NORFOLK & PORTSMOUTH BELTLINE RAILROAD
VARIABLE R/W

NORFOLK HARBOR
CHANNEL LIMITS
MAINTAINED DEPTH 45'

SOUTHERN BRANCH OF THE
ELIZABETH RIVER

VIRGINIA STATE PLANE
SOUTH ZONE
NAD 1983



POST DEVELOPMENT DRAINAGE MAP
PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA	MADE FOR: PER PROPERTIES
DESIGN BY: BWG	DRAWN BY: JB
CHECKED BY: BWG	DATE: OCTOBER 2, 2013
SCALE: 1" = 60'	SHEET 3/13
DATE	COMMENT
REVISION	SCHEDULE

GALLUP
SURVEYORS & ENGINEERS, LTD.
323 FIRST COLONIAL ROAD
VIRGINIA BEACH, VIRGINIA 23454
(757)428-8132 (757)425-2390 FAX

C3

NOTE:
ALL BUILDING STRUCTURES ARE FUTURE
AND ARE TO BE APPROVED SEPARATELY.



MATCH LINE SEE SHEET C4



SOUTHERN BRANCH OF THE ELIZABETH RIVER

SHIP MOORING (TYPICAL)

SHEETPILE BULKHEAD TOP 10.50 (BY OTHERS)

CONCRETE SURFACE

35' DOCK

INV -1.23

INV -2.50

BARGE HOPPER

STMH-8

STMH-7

STMH-6A

DI-9A

DI-8A

BUILDING ONE
FF=12.00

36' DIA. TANK (TYP.)
FG BASE 12.00

36'x100' SHOP
FF=12.00

DI-10A

DI-10

STMH-2

STMH-3

STMH-4

STMH-5

VEPCO
15' UTILITIES & MAINTENANCE EASEMENT
D.B. 842, PG. 82

PROPOSED RETAINING WALL
TW=10.50

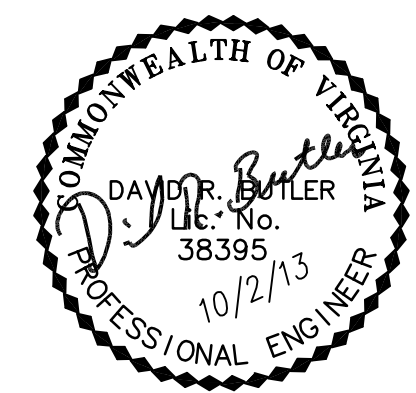
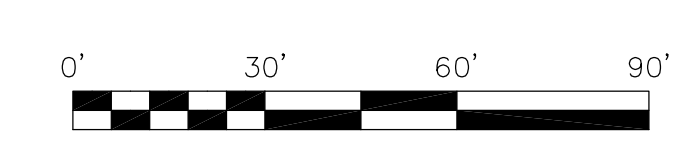
PROVIDE 3 S.Y. OF EC-1 STONE OVER FILTER FABRIC

THE AREA BETWEEN THE PROPOSED BERM AND THE SOUTHERN BOUNDARY LINE WILL BE FILLED, BY OTHERS, WITH THE ATLANTIC WOOD SUPERFUND PROJECT.

FUTURE FINISHED GRADE CONTOUR-EPA (TYP.)

FUTURE OFFSHORE SHEET PILE WALL (BY OTHERS) TW10.50

ELM AVENUE STATE ROUTE NO. 337 (VARIABLE R/W)



GRADING PLAN AND UTILITY PLAN
PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 30'	SHEET 5/13

C5

PIPE SCHEDULE

10–10A
208°–24° HDPE @ 0.25%
INV IN 4.77, INV OUT 4.25
10A–11
207°–24° HDPE @ 0.25%
INV IN 4.25, INV OUT 3.73
11–12
198°–24° HDPE @ 0.20%
INV IN 3.73, INV OUT 3.33
12–12A
59°–24° HDPE @ 0.34%
INV IN 3.33, INV OUT 3.13
12A–13
191°–24° HDPE @ 0.34%
INV IN 3.13, INV OUT 2.49
RR–13
117°–12° HDPE @ 1.03%
INV IN 8.50, INV OUT 7.29
9A–8A
109°–18° PERFORATED HDPE @ 0.60%
INV IN 4.09, INV OUT 3.44
15–14
89°–18° HDPE @ 0.30%
INV IN 3.23, INV OUT 2.96

14-13
 196"-24" HDPE @ 0.24%
 INV IN 2.96, INV OUT 2.49
 13-7A
 215"-18" PERFORATED HDPE @ 0.23%
 INV IN 2.49, INV OUT 2.00
 7A-6
 344"-36" CL. IV RCP @ 0.62%
 INV IN 4.00, INV OUT 1.87
 8A-7A
 215"-24" CL. IV RCP @ 0.67%
 INV IN 3.44, INV OUT 2.00
 5A-6
 330"-15" HDPE @ 0.51%
 INV IN 5.09, INV OUT 3.41
 6-OUTLET
 144" 42" HDPE @ 0.50%
 INV IN -0.58, INV OUT -1.30
 PROVIDE TIEFLEX TP-1
 ON OUTLET END

4-5
150'-36" HDPE @ 0.15%
INV IN -0.14, INV OUT -0.37

5-6A
154'-36" HDPE @ 0.13%
INV IN -0.37, INV OUT -0.57

6A-7
220'-36" HDPE @ 0.13%
INV IN -0.57, INV OUT -0.86

7-8
158'-36" HDPE @ 0.12%
INV IN -0.86, INV OUT -1.05

8-OUTLET
152'-36" HDPE @ 0.12%
INV IN -1.05, INV OUT -1.23
PROVIDE TIDEFLEX TF-1
ON OUTLET END

1A-1
134°-12" HDPE @ 0.10%
INV IN 4.36, INV OUT 4.23

1-2
119°-30" HDPE @ 0.17%
INV IN 4.23, INV OUT 4.04

2-3
204°-30" HDPE @ 0.15%
INV IN 4.04, INV OUT 3.73

3-4
156°-30" HDPE @ 0.15%
INV IN 3.73, INV OUT 3.50

AT STMH-2:
10°-18" HDPE WITH 18" FES
INV IN 5.50, INV OUT 4.04

AT STMH-4:
6'-36" HDPE WITH 36" FES
INV IN 2.85, INV OUT 2.50

AT STMH-3:
10'-18" HDPE WITH 18" FES
INV IN 4.80, INV OUT 3.73

AT STMH-1A:
10'-12" HDPE WITH 12" FES
INV IN 5.90, INV OUT 4.36

AT STMH-1:
10'-30" HDPE WITH 30" FES
INV IN 5.80, INV OUT 4.23

PEOLK &

10'-18" HDPE WITH 18" FES
INV IN 4.80, INV OUT 3.73

AT STMH-1A:
10'-12" HDPE WITH 12" FES
INV IN 5.90, INV OUT 4.36

AT STMH-1:
10'-30" HDPE WITH 30" FES
INV IN 5.80, INV OUT 4.23

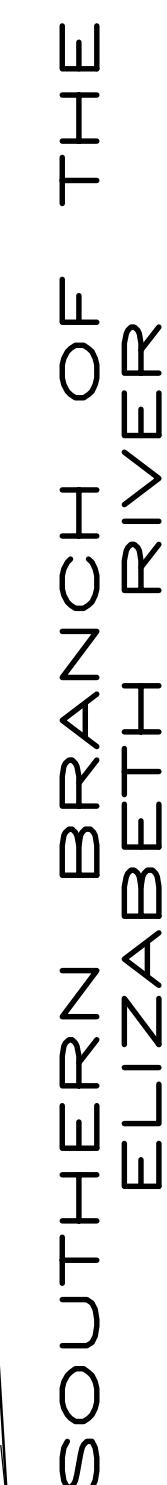
ROCKFORD & PORTSMOUTH BELTLINE RAILROAD
VARIABLE R/W

PROPOSED
STATIONING
RIGHT OF WAY

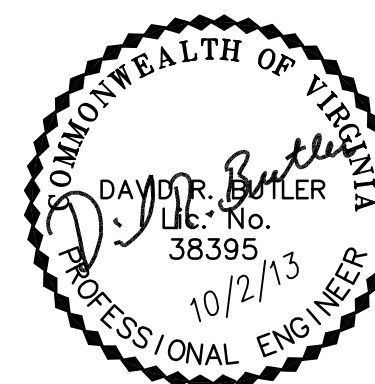
POPEL &

THE INVERTS SHOWN ON THE DROP INLET DENOTES THE INVERT OF THE PIPES. PROVIDE A 12" DEEP SUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS FOR MAINTENANCE PURPOSES FOR STRUCTURES 7A, 8A, 9A, AND 13.

ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING.
FINAL SURFACE WILL BE GRAVEL AND CRUSHED CONCRETE




VIRGINIA STATE PLANE
SOUTH ZONE
NAD 1983



OVERALL SITE PLAN

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA			MADE FOR: PER PROPERTIES		
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013		
 <p>GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX</p>			SCALE: 1" = 60'	SHEET	C3
			FILE NO.: 81-32	3/13	

AREA SUMMARY:

C FACTOR FOR ROOF AND CONCRETE=0.90
C FACTOR FOR GRAVEL=0.70
C FACTOR FOR GRASS=0.30

DRAINAGE CALCULATIONS
FOR PER, LOCATED IN
CITY OF PORTSMOUTH
REVISED AUGUST 2013

AREA 1:

A TOTAL=25,685 SQ. FT. = 0.5896 AC.
3588 S.F.=0.0823 AC. X 0.9 = CA=0.0741
5794 S.F. = 0.1330 AC. X 0.3 = CA=.0399
16303 S.F.=0.3743 AC X 0.70 = CA=0.2691
SUM CA'S=0.3760, C=0.6377

AREA 2:

A TOTAL=33030 S.F.=0.7583 AC.
20626 S.F.=0.4735 AC X 0.90=0.4262
12404 S.F.=0.2848 A. X 0.70=0.1993
SUM CA=0.6255, C=0.8249

AREA 3:

64176 S.F.=1.4733 AC.
22740 S.F.=0.5220 AC. X 0.9=0.4688
41436 S.F.=0.9512 AC. X 0.7=0.6659
SUM CA=1.1357, C=0.7708

AREA 4 TO STUB:

5616 S.F. = 0.1289 X 0.70=0.0902

AREA 5:

A TOTAL = 47804 S.F. = 1.0974 AC.
7635 S.F.=0.1753 AC. X 0.9=0.1577
40,169 S.F. = 0.9222 AC. X 0.7=0.6455
SUM CA=0.8032, C=0.7319

AREA 6:

AREA TOTAL=35,545 S.F.=0.816 AC.
14029 S.F. = 0.3221 AC. X 0.9=0.2899
21516 S.F.=0.494 AC. X 0.7=0.3457
SUM CA=0.6357, C=0.779

AREA 7:

AREA TOTAL=60,483 S.F.=1.3885 AC.
3604 S.F. = 0.0827 X 0.9=.0745
56,879 S.F.=1.3058 AC. X 0.7=0.914
SUM CA=0.9885, C=0.7119

AREA 8:

AREA TOTAL=71818 S.F.=1.6510 AC.
9608 S.F.=0.2206 AC. X 0.90=0.1985
62310 S.F.=1.4304 AC. X 0.7=1.0013
SUM CA=1.1998, C=0.7267

AREA 9:

AREA TOTAL=95,890 S.F.=2.2013 AC.
14484 S.F.=0.3325 AC. X 0.9=0.2993
81406 S.F.=1.8688 AC. X 0.7=1.3082
SUM CA=1.6075, C=0.73

AREA 10:

37065 S.F.=0.8509 AC.
C=0.7, CA=0.5956

AREA 11:

AREA TOTAL=33263 S.F.=0.7636 AC.
11374 S.F.=0.2611 AC. X 0.9=0.235
21889 S.F.=0.5025 AC. X 0.7=0.3518
SUM CA=0.5867, C=0.7684

AREA 12:

AREA TOTAL=110476 S.F.=2.5361 AC.
1903 S.F.=0.0436 X 0.9=0.0393
108573 S.F.=2.4924 AC. X 0.7=1.7447
SUM CA=1.7841, C=0.7034

OFFSITE AREAS FROM DIXON TRACT:

TO STMH-1A

AREA TOTAL=3199 S.F.=0.0735 AC.
3199 S.F.=0.0735 AC. X 0.5=0.0368

TO STMH-1

AREA TOTAL=85581 S.F.=1.9646 AC.
1672 S.F.=0.0384 AC. X 0.5=0.0192
83909 S.F. = 1.9262 AC. X 0.90=1.7337
SUM CA=1.7529, C=0.8922

TO STMH-2

AREA TOTAL=1529 S.F.=0.0351 AC. X 0.5=.0175

TO STMH-3

AREA TOTAL=2239 S.F.=0.0514 AC. X 0.5=.0257

TO STMH-4

AREA TOTAL=53466 S.F.=1.2274 AC. X 0.9=1.1047

C FACTORS FOR THE DIXON TRACT ASSUME
ULTIMATE DEVELOPMENT:

SUM OF THE OFFSITE AREAS=146,014 S.F. = 3.352 AC.
SUM OF THE OFFSITE CA's=2.93755
ULTIMATE C FACTOR = 2.9376/3.3520 = 0.88

OFFSITE STORM SEWER IS DESIGNED WITH THE
DIXON TRACT BEING ULTIMATELY DEVELOPED,
NOT THE CURRENT STATE (CONSERVATIVE)

NOTES:

ONSITE AND OFFSITE DRAINAGE DESIGNED FOR
THE 100 YEAR STORM. BOTH SYSTEMS ARE
INDEPENDENT AND SEPARATE. WATER QUALITY
STORAGE CALCULATIONS WERE PERFORMED BASED
ON ONE INCH OF RUNOFF OVER THE IMPERVIOUS
AREAS WITHIN THE REQUIRED DRAINAGE AREA.
PEAK RUNOFF WILL BE REDUCED SOMEWHAT
BECAUSE OF INFILTRATION WITH THE BMP TRENCH,
BUT WAS NOT CONSIDERED IN THE STORM DRAIN
DESIGN.

WATER QUALITY CALCULATIONS FOR INFILTRATION TRENCH

AREA 8:
TOTAL AREA=1.651 AC.
ROOF A=0.2206 AC.
GRAVEL AREA=1.4304 AC, 70% IMPERVIOUS=1.0013 AC.
SUM=1.2219 AC.

AREA 9:
TOTAL AREA=2.2013 AC.
ROOF A=0.3325 AC.
GRAVEL AREA =1.8688 AC., 70% IMPERVIOUS = 1.3082 AC.
SUM=1.6407 AC.

AREA 3:
TOTAL AREA=1.4733 AC.
ROOF A=0.522 AC.
GRAVEL AREA=0.9512 AC.. 70% IMPERVIOUS=0.6659 AC.
SUM=1.1879 AC.

AREA 11:
TOTAL AREA=0.7636 AC.
ROOF A=0.2611 AC.
GRAVEL AREA=0.5025 AC, 70% IMPERVIOUS=0.3518
SUM=0.6129 AC.

AREA 2:
TOTAL AREA=0.7583 AC.
ROOF A=0.4735 AC.
GRAVEL A=0.2847 AC, 70% IMPERVIOUS = 0.1993 AC.
SUM=0.6728 AC.

AREA 5:
TOTAL A=1.0974 AC.
ROOF A=0.1753 AC.
GRAVEL A=0.9222 AC., 70% IMPERVIOUS = 0.6455 AC.
SUM=0.8208

AREA 1:
TOTAL AREA=0.5896 AC.
ROOF A=0.0823 AC.
GRAVEL A=0.3743 AC, 70% IMPERVIOUS=0.2619 AC.
SUM=0.3442 AC.

SUM OF THE AREAS=8.5344 AC.
SUM OF THE IMPERVIOUS AREAS=6.5012 AC.
I% = 6.5012 AC./8.5344 AC. = 76.2%

REQUIRED VOLUME IS 1" X WATER QUALITY VOLUME:
 $(0.5"/12)(6.5012 \text{ AC.}) (43,560 \text{ S.F./AC.}) = 11,799 \text{ CUBIC FEET}$

TRENCH INSTALLED BETWEEN 13 AND 9A:
LENGTH=544 L.F.
DEPTH OF 57 STONE=4'
WIDTH OF TRENCH=13.67'
VOID VOLUME IS 40% OF TOATL VOLUME
VOLUME PROVIDED IN VOIDS=(544')(4')(13.67')(0.4) = 11,898 C.F. > 11,799 C.F.

BMP AREA FOR TABLE ON COVER SHEET:
838.8' X 4' DEEP X 2 SIDES = 4,310 S.F.
27.3' WIDE X 4' DEEP X 2 SIDES = 55 S.F.
1,143 S.F. BOTTOM AREA
TOTAL=5,508 S.F.

FROM BMP CLEARINGHOUSE:

INFILTRATION PRACTICE NUMBER 8, TOTAL MASS LOAD REMOVAL OF TOTAL PHOSPHORUS = 50%

APPLICABLE AREA=14.87 ACRES

1 WATERSHED FOR PORTSMOUTH=54%

EXISTING IMPERVIOUS AREA=1.15 ACRES

USE SITUATION 2, PERFORMANCE BASED WATER QUALITY CALCULATIONS

1 EX.< 1 WATERSHED

1 POST> 1 WATERSHED

$L_{PRE} (WS) = (0.05 + (0.009 \times 54)) \times 14.87 \text{ AC.} \times 2.28 = 18.2 \text{ LBS/YEAR}$

$L_{POST} = (0.05 + (0.009 \times 76.6)) \times 14.87 \times 2.28 = 25.06 \text{ LBS/YR.}$

$RR = L_{POST} - L_{PRE}$

$RR = 25.06 - 18.2 = 6.9 \text{ LBS/YR.}$

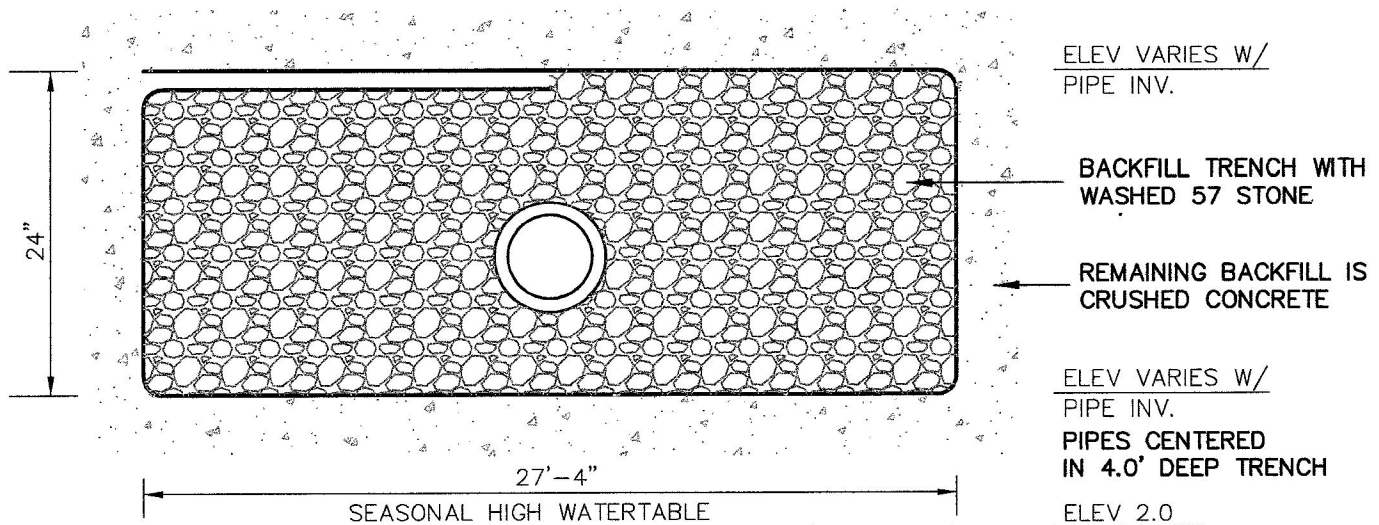
USING INFILTRATION,

$L_{BMP} = (0.05 + (0.009 \times 76.2)) \times 8.5344 \times 2.28 = 14.31 \text{ LBS/YR.}$

$L_{REMOVED \text{ BY BMP}} = 0.50 \times 14.31 = 7.15 \text{ LBS/YR}$

$7.2 \text{ LBS/YR} > 6.9 \text{ LBS/YR}$

WATER QUALITY IS SATISFIED.



TRENCH LENGTH=544 L.F.

INFILTRATION RATE (I)=0.0000713 F/S

VOLUME=L x W x D x 0.4

VOID VOLUME = 40% OF TRENCH VOLUME

Q OUT=I x TOTAL TRENCH AREA

VOID RATIO OF 57 STONE: 0.40

VOID VOLUME OF CRUSHED CONCRETE: 0.30-0.40

TRENCH INSTALLED BETWEEN 13 AND 9A:

LENGTH=544 L.F.

DEPTH OF 57 STONE=2'

WIDTH OF TRENCH=27.34'

VOID VOLUME IS 40% OF TOTAL VOLUME

VOLUME PROVIDED IN VOIDS=(544')(2')(27.34')(0.4) = 11,898 C.F. > 11,799 C.F.

TRENCH AREA: (2' x 544' x 2 SIDES) + (27.34' x 544' x 2) = 31,922 S.F.

0.0000713 F/S x 31,922 S.F. = 2.28 CFS

Q IS REDUCED BY 1.37 CFS

2 YEAR STORM VOLUME FROM HYDROGRAPH=40,561 C.F.

Q OUT=0.0000713 C.F/S PER S.F. x 31,922 S.F. = 2.276 CF/SEC

40,561 C.F./2.276 CFS = 17,821 SEC x 1 MIN/60S x 1 HR./60 MIN x 1 DAY/24 HOURS = 0.21 DAYS

2 YEAR STORM WILL EXFILTRATE IN 0.21 DAYS

INLET CAPACITY CALCULATIONS

CALCULATIONS PERFORMED USING VDOT GRATE INLET CAPACITY CHART

WIDTH OF STANDARD DROP INLET = 2.17, LENGTH = 2.17'

EQUATION FOR CHART NOMOGRAPH: $P=2(W+L)$;

FOR SINGLE INLET, $P=2(2.17'+2.17')=8.68$

DI-10

Q100=5.63 CFS

DEPTH AT INLET=0.38'

ELEVATION AT INLET=RIM ELEVATION + DEPTH = $9.80+0.38'=10.18'<10.5$

STORM IS CONTAINED

DI-11

Q=0.7583 X 0.8249

TC=5 MINS.

I100 = 9.60 IN/HR

Q100=6.01 CFS

DEPTH=0.39'

ELEV.=0.39'+9.80=10.19 < 100.50

DI-12

TC=10 MINS

I100=8.21

Q100 = $0.5896 \times 0.6377 \times 8.21 = 3.1$ CFS

DEPTH AT INLET=0.24'

ELEVATION = $0.24'+9.50=9.74' < 10.5$

DI-13

T=10 MINS

I100=8.21

Q100= $1.0974 \times 0.7319 \times 8.21 = 6.6$ CFS

DEPTH AT INLET = 0.41'

ELEVATION = $0.41'+9.35=9.76 < 10.5$

DI-14

TC=5 MINS

I100=9.60

Q100= $1.3885 \times 0.7119 \times 9.60 = 9.5$ CFS

DEPTH AT INLET = 0.52'

ELEVATION = $0.52'+9.35 = 9.87' < 10.5$

DI-15

TC=5 MINS

I100=9.60

Q100= $0.816 \times 0.779 \times 9.60 = 6.1$ CFS

DEPTH AT INLET=0.39'

ELEVATION= $0.39'+9.35 = 9.74 < 10.5$

DI-8A

TC=15.32 MIN

I100=7.13

Q100= $2.2013 \times 0.73 \times 7.13 = 11.5$ CFS

DEPTH AT INLET=0.59'

ELEVATION= $0.59'+9.60 = 10.19' < 10.5$

DI-7A

TC=5 MINS

I100=9.60

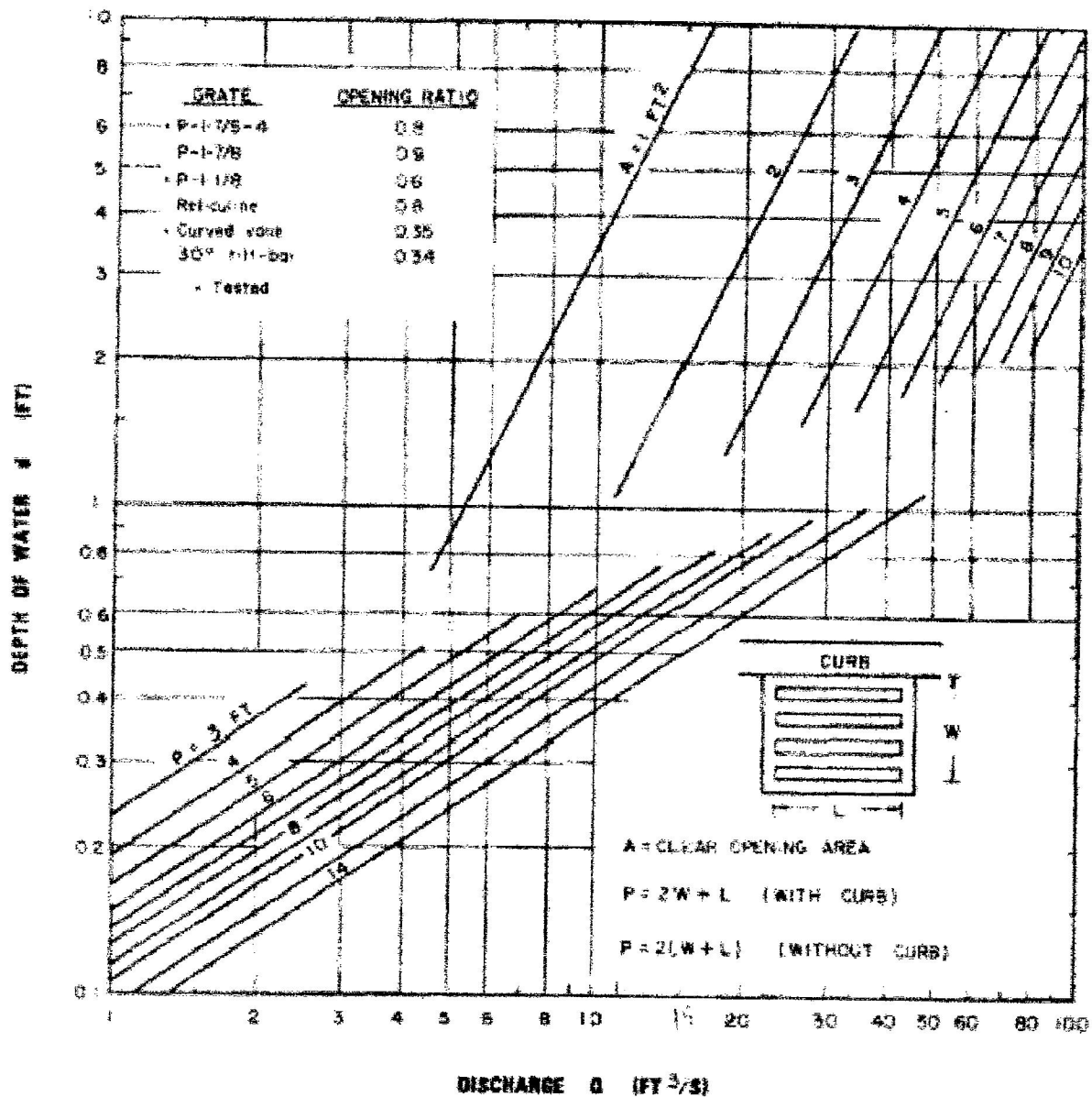
Q100= $1.4733 \times 0.7708 \times 9.60 = 10.9$ CFS

DEPTH AT INLET = 0.57'

ELEVATION= $0.67'+9.50 = 10.17 < 10.5$

endix 9C-12

Grate Inlet Capacity in Sump Conditions



Grate Inlet Capacity in Sump Conditions - English Units

FOR HGL CALC'S, THE STARTING HW ELEV.
USED IS MHW (NAV. 88), ELEV=1.10
AT EACH UPSTREAM INLET, BEGINING TW ELEV.
IS EITHER LAST HGL ELEV, DEPTH IN PIPE
CONVERTED TO ELEV, OR CRITICAL DEPTH
CONVERTED TO ELEV. IN ALL CASES, THE LAST HGL
ELEV IS THE CONTROL.

CHECK CONTROL FOR OFFSITE HGL CALC'S:

DEPTH IN PIPE AT NO. 8 USING 24.87 CFS, $S=0.0012 = 2.44'$, ELEV. $= -1.05+2.44'=1.39$, USE 1.42
DEPTH IN PIPE AT NO. 7 USING 25.54 CFS, $S=0.0013 = 2.41'$, ELEV. $= -0.86+2.41'=1.55$, USE 1.74
DEPTH IN PIPE AT NO. 6A USING 26.02 CFS, $S=0.0013 = 2.47'$, ELEV. $= -0.57+2.47'=1.90$, USE 2.17
DEPTH IN PIPE AT NO. 5 USING 26.34 CFS, $S=0.0036 = 1.69'$, ELEV. $= -0.37+1.69'=1.32$, USE 2.51
DEPTH IN PIPE AT NO. 4 USING 16.75 CFS, $S=0.0015 = 1.99'$, ELEV. $= 3.51+1.99=5.50$, USE 5.50
DEPTH IN PIPE AT NO. 3 USING 16.98 CFS, $S=0.0015 = 2.02'$, ELEV. $= 3.73+2.02=5.75$, USE 5.83
DEPTH IN PIPE AT NO. 2 USING 17.11 CFS, $S=0.0016 = 1.97'$, ELEV. $= 4.04+1.97=6.01$, USE 6.26
DEPTH IN PIPE AT NO. 1 USING 0.35 CFS, $S=0.0010 = 0.37'$, ELEV. $= 4.24+0.37=4.61$, USE 6.52

July 2000

$$I_{100} = \frac{285.2}{24.7 + T_c}$$

MLW (NAV 39) = 1.10
MLW = -1.66 ROI

STORM SEWER DESIGN COMPUTATIONS

ROUTE: _____ PROJ: PER PROSPECTIVE OCT 12, 2013
COUNTY: _____ DISTRICT: _____
DESCRIPTION: _____

OFFSITE

SHEET OF

[illegible]

HYDRAULIC GRADE LINE

OFFSITE

BEGIN TW Elev. MIN = 1.0

PROJECT: PER PROPERTIES

05/12/2013

JUNCTION LOSS

INLET STATION	Outlet Water Surface Elev.	D _o	Q _o	L _o	S _f %	H _f	V _o	H _o	Q _i	V _i	QV _i	V _i ² 2g	H _i	Angle	H _A	H _t	1.3 H _t	0.5 H _t	Final H	Inlet Water Surface Elev.	Rim Elev.
3	1.10	36"	24.40	152	.134	.203	4.04	.063	24.87	4.04	102.47	.0584	.089	53°	.021	.24	-	.12	.33	1.42	10.50
7	1.42	36"	24.87	153	.139	.219	4.20	.063	25.64	4.20	107.27	.274	.090	17°	.034	.193	-	.10	.52	1.74	10.50
6A	1.74	36"	25.54	220	.147	.3225	4.20	.0685	26.02	4.20	109.28	.274	.090	25°	.060	.225	-	.11	.43	2.17	10.50
5	2.17	36"	26.02	154	.152	.234	4.20	.068	26.34	4.60	113.53	.314	.1101	17.5°	.041	.219	-	.11	.34	2.51	10.50
4	2.51	36"	26.34	150	.150	.233	4.60	.079	16.75	3.99	66.38	.247	.089	90°	.173	.333	-	.17	.40	2.91	10.50 *
3	5.50	36"	16.75	150	.167	.26	3.99	.062	16.93	4.00	67.92	.248	.087	0°	-	.149	-	.074	.33	5.83	10.50/5.9
2	5.83	36"	16.93	204	.171	.349	4.00	.062	17.11	4.12	70.49	.264	.092	0°	-	.150	-	.08	.43	6.26	10.50/6.9
1	6.26	36"	17.11	126	.174	.219	4.12	.065	0.35	1.34	0.47	.028	.0098	0°	-	.076	-	.04	.26	6.52	10.50/6.9
1A	6.52	12"	0.35	129	.010	.012	1.34	.007	-	-	-	-	-	0°	-	.007	-	.02	.004	6.54	10.50/7.4

DEPT 6 e 8 using 24.87 cfs, S_o = .0012 = 2.44' Elev. = -1.05 + 2.44 = 1.39DEPT 7 using 25.54 cfs, S_o = .0013 = 2.41' Elev. = -0.86 + 2.41 = 1.55DEPT 6 using 26.02 cfs, S_o = .0013 = 2.41' Elev. = -0.57 + 2.41 = 1.90DEPT 5 using 26.34 cfs, S_o = .0030 = 1.69 Elev. = -0.37 + 1.64 = 1.32 (use 2.51)DEPT 4 using 16.75 cfs, S_o = .0015 = 2.30' elev. = 1.99 + 1.99 = 6.60, use 5.50DEPT 3 using 16.93 cfs, S_o = .0015 = 2.30' elev. = 1.99 + 1.99 = 6.60, use 5.50DEPT 2 using 17.11 cfs, S_o = .0015 = 2.30' elev. = 1.99 + 1.99 = 6.60, use 5.50DEPT 1 using 17.11 cfs, S_o = .0015 = 2.30' elev. = 1.99 + 1.99 = 6.60, use 5.50

50° K = 0.50 20° K = 0.25
 40° K = 0.43 15° K = 0.19
 30° K = 0.35 10° K = 0.13
 25° K = 0.30 5° K = 0.06
 * Elev. 2.9 = Ex. Elev. on
 2.50 and property
 (6000)

MHW ELEV. = 1.1005
MLW ELEV. = -1.6554
LD-229
AVG. =
July 2000

ON-SITE DRAINAGE

STORM SEWER DESIGN COMPUTATIONS

ROUTE: _____ PROJ: PER PROPERTIES
COUNTY: _____ DISTRICT: REV. AUG. 2013
DESCRIPTION: _____

SHEET _____ OF _____

$I_{.002} = 285.2/4.7 = 7.2$

FROM POINT	TO POINT	AREA DRAIN "A"	RUN-OFF COEFF.	CA		INLET TIME	RAIN FALL	RUN-OFF Q	INVERT ELEVATIONS		LENGTH	SLOPE	DIA.	CAPA-CITY	VEL.	FLOW TIME MIN.	REMARKS
		ACRES	C	INCRE-MENT	ACCUM-ULATE	MIN-UTES	IN./HR.	C.F.S.	UPPER END	LOWER END	FT.	FT./FT.	IN.	C.F.S.	F.P.S.		
10	11	.7636	.7684	.5837		5	9.60	5.63	4.77	3.73	417'	.0025	24"	12.25	3.82	1.82	(V10)
11	12	.7583	.8249	.6255	1.2123	6.39	9.03	10.94	3.73	3.33	198'	.0020	24"	10.96	3.49	0.83	✓
12	12A				1.2123	7.72	8.30	13.93	3.33	3.13	59'	.0034	24"	14.29	5.18	0.19	✓
12A	13	.5346	.6377	.376	1.5833	7.91	8.75	13.89	3.13	2.49	191'	.0034	24"	14.29	5.18	0.61	✓
																	✓
RR TRAILS	13	.1234	.70	.0902		10	8.22	0.74	8.50	7.29	117'	.0103	12"	3.92	3.33	0.51	
9A	8A	1.651	.7267	1.1948		15	7.13	8.61	4.09	3.44	109'	.0060	18"	3.81	5.63	0.32	✓
8A	7A	2.2013	.73	1.6055	2.3553	15.32	7.13	20.01	3.44	2.00	215'	.0007	24"	20.06	6.33	0.49	✓
15	14	.816	.779	.6357		8.5	8.59	5.46	3.23	2.96	89'	.0030	18"	6.23	3.93	.37	✓
14	13	1.3335	.7117	.9335	1.6242	8.87	8.47	13.79	2.96	2.49	196'	.0024	24"	13.86	5.03	.65	✓
13	7A	1.0974	.7317	.3032	4.1059	9.52	8.33	34.22	2.49	2.00	215'	.0023	30"	34.65	5.59	.64	✓
7A	6	1.4733	.7703	1.1356	8.0433	15.81	7.04	56.67	4.00	1.87	344'	.0062	36"	56.39	9.13	.62	✓
5A	6	.8507	.70	.5956		9.50	8.34	4.97	5.09	3.41	330'	.0051	15"	5.00	4.64	1.19	✓
6	OUT	2.5361	.7034	1.7339	10.4233	10.47	6.93	72.27	-0.58	-1.30	144'	.005	42"	77.07	9.11	.26	✓

10 10A .5867 5 9.60 5.63 4.77 4.25 208' .0025 24" 12.25 3.82
10A 11 .5367 8 9.60 5.63 4.25 3.73 207' .0025 24" 12.25 3.82

INLET STATION	Outlet Water Surface Elev.	D _o	Q _o	L _o	S _f %	H _f	JUNCTION LOSS												Final H	Inlet Water Surface Elev.	Rim Elev.
							V _o	H _o	Q _i	V _i	Q _v V _i	$\frac{V_i^2}{2g}$	H _i	Angle	H _Δ	H _t	1.3 H _t	0.5 H _t			
6	1.10	42"	72.27	144	.516	.74	9.11	.32	56.67	9.18	520.23	1.31	.46	1°	.01	.79	1.03	.51	1.26	2.36	9.70
5	2.67	15"	4.97	330	.592	1.95	4.64	.084	-	-	-	-	-	-	-	.084	.109	.05	2.00	4.67	9.70
7A	2.67	36"	56.67	344	.722	2.43	9.13	.327	72.27	10.22	733.6	1.62	.567	90°	1.14	2.03	2.64	3.80	3.80	6.47	9.70
13	6.47	30"	34.22	215	.696	1.49	5.59	.121	12.93	5.11	71.44	.41	.14	0°	-	.26	.342	.17	1.67	8.14	9.70
12	8.14	24"	13.93	254	.382	.97	5.11	.10	10.94	3.49	38.18	.19	.07	89°	.13	.30	.39	.19	1.16	9.30	9.70
11	9.30	24"	10.94	198	.234	.46	3.49	.05	5.63	3.67	20.66	.21	.07	0°	-	.12	.16	.08	.54	9.84	10.00
10	9.84	24"	5.63	417	.062	.26	3.82	.06	-	-	-	-	-	-	-	.06	.07	.04	.295	10.13	10.13
8A	6.47	24"	20.01	215	.732	1.68	6.38	.16	8.61	5.68	43.2	.50	.13	23°	.10	.43	.56	.23	1.90	8.30	
9A	8.30	18"	8.61	104	.671	.731	5.02	.13	-	-	-	-	-	-	-	.13	.16	.03	.81	9.61	

$H_i = 0.35 V_i^2 / 2g$; $H_o = 0.25 V_o^2 / 2g$; $H_{\Delta} = K V_i^2 / 2g$; $H_t = H_o + H_i + H_{\Delta}$

FINAL H = H_f + H_t

90° K = 0.70	50° K = 0.50	20° K = 0.25
80° K = 0.66	40° K = 0.43	15° K = 0.19
70° K = 0.61	30° K = 0.35	10° K = 0.13
60° K = 0.56	25° K = 0.30	5° K = 0.06

344

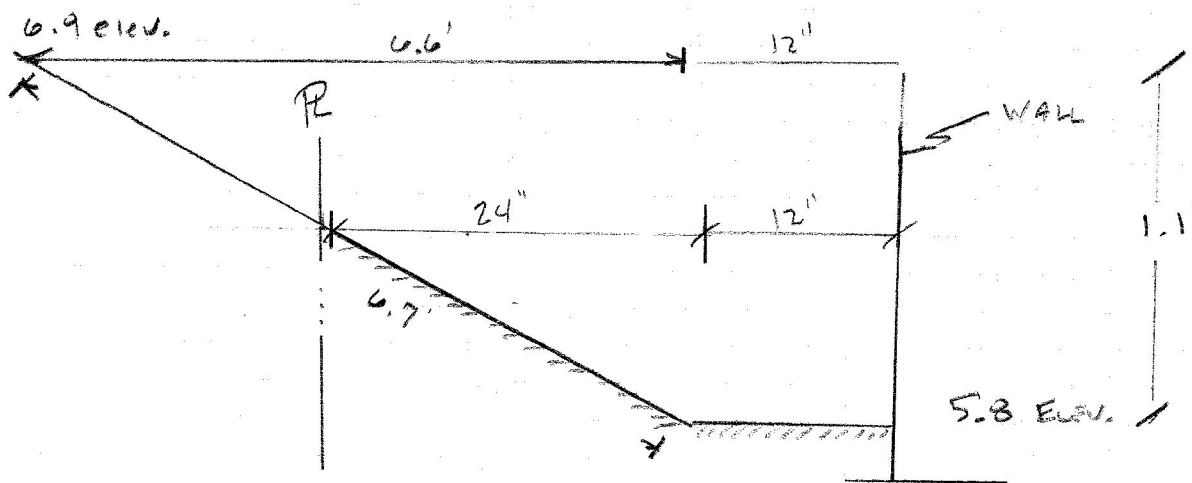
CHECK DITCH CAPACITY NEAR STMH-1

$$Q_{100} = CAI$$

$$= (0.5)(1.0384)(10.0) = 0.19 \text{ cfs}$$

30" FES DOWNSTREAM
TO PICK UP OPPOSITE RUNOFF

FORM LD-269 SHOWS HW DENTAS 0.37', ELEV. = 6.07, TOP BANK = 6.9



$$XS = (6.9 - 5.8)(1.0) = 1.1 \text{ ft}^2$$

$$+ 0.5 \times 6.6' \times 1.1' = 3.63 \text{ ft}^2 / \Sigma = 4.73$$

$$W.P. = 6.7 \times 1.02 = 7.7$$

$$R = 4.73 / 7.7 = 0.61$$

n FACTOR = 0.45, DENSE GROWTH, $S_o = 0.005 \text{ F/F}$

$$Q_{cap.} = 1.486 / n A R^{2/3} S_o^{1/2}$$

$$= (1.486 / 0.45)(4.73)(0.61)^{0.67}(0.005)^{0.5}$$

$$= 0.79 \text{ cfs} > 0.19 \text{ cfs}$$

CULVERTS

[illegible]

ENTRANCE LOSS COEFFICIENTS (K_e) OUTLET CONTROL, FULL OR PARTIALLY FULL

Type of Structure and Design of Entrance	Coefficient
Pipe, Concrete	
Mitered to conform to fill slope	0.7
End-section conforming to fill slope	0.5
Projecting from fill, square cut end	0.5
Headwall or headwall and wingwall	
Square-edge	0.5
Rounded (radius = 1/12 D)	0.2
Socket end of pipe (groove end)	0.2
Projecting from fill, socket end (groove end)	0.2
Beveled edges, 33.7° or 45° bevels	0.2
Side or slope-tapered inlet	0.2
Pipe, Corrugated Metal (or Corrugated HDPE)	
Projecting from fill (no headwall)	0.9
Mitered to conform to fill slope, paved or unpaved slope	0.7
Headwall or headwall and wingwall, square-edge	0.5
End section conforming and to fill slope	0.5
Beveled edges, 33.7° or 45° bevels	0.2
Side or slope-tapered inlet	0.2
Box, Reinforced Concrete	
Wingwalls parallel (extension of sides), square edged at crown	0.7
Wingwalls at 10° to 25° or 30° to 75° to barrel, square edged on 3 edges	0.5
rounded on 3 edges to radius of 1/12 barrel	0.2
Wingwalls at 30° to 75° to barrel, crown edge rounded to radius 1/12 of barrel	0.2
Side or slope-tapered inlet	0.2

Note:

End Section conforming to fill slope made of metal, concrete, or HDPE, are the sections commonly available from manufacturers. From limited hydraulic test they are equivalent in operation to a headwall in both inlet and outlet control. Some end sections incorporating a closed taper in their design have a superior hydraulic performance. These latter sections can be designed using the information given for the beveled inlet.

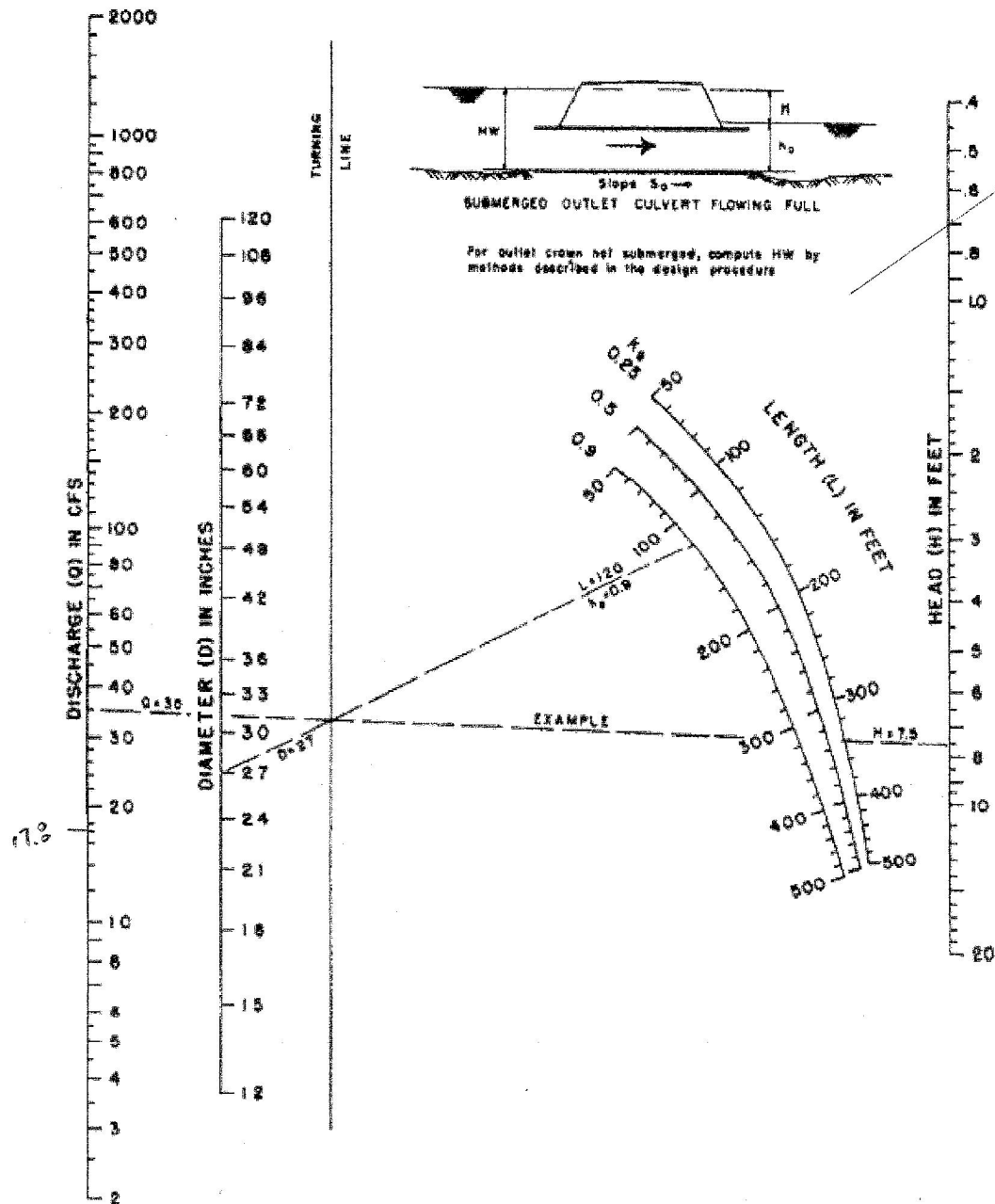
OUTLET CONTROL, CIRCULAR CONCRETE PIPE RECOMMENDED MANNING'S n-VALUES

Type of Conduit	Wall Description	Manning's n
Concrete Pipe	Smooth walls	0.010 - 0.013
Concrete Boxes	Smooth walls	0.012 - 0.015
Corrugated Metal	2 2/3 by 1/2 inch	0.022 - 0.027
Pipes and Boxes, Annular or	corrugations	
Helical Pipe	6 by 1 inch	0.022 - 0.025
	corrugations	
	5 by 1 inch	0.025 - 0.026
	corrugations	
	3 by 1 inch	0.027 - 0.028
	corrugations	
	6 by 2 inch	0.033 - 0.035
	structural plate	
	9 by 2 1/2 inch	0.033 - 0.037
	structural plate	
Corrugated Metal	2 2/3 by 1/2 inch corrugations	0.012 - 0.024
Pipe		
Spiral Rib Metal	Smooth walls	0.012-0.013
(Steel or Alum.)		
PVC	Smooth interior	0.010 - 0.012
Polyethylene (PE or HDPE)	Smooth interior	0.011 - 0.013
Corrugated PE or HDPE	Corrugated interior	0.022 - 0.026

Note 1: The values indicated in this table are recommended Manning's "n" design values. Actual field values may vary depending on the effects of abrasion, corrosion, deflection, and joint conditions. Concrete pipe with poor joints and deteriorated walls may have "n" values of 0.014 to 0.018. Corrugated metal with joint and wall problems may also have higher "n" values, and in addition, may experience shape changes which could adversely affect the general hydraulic characteristics of the culvert.

Note 2: For further information concerning Manning n values for selected conduits consult Hydraulic Design of Highway Culverts, Federal Highway Administration, HDS No. 5, page 163.

OUTLET CONTROL, CIRCULAR CORRUGATED METAL PIPE



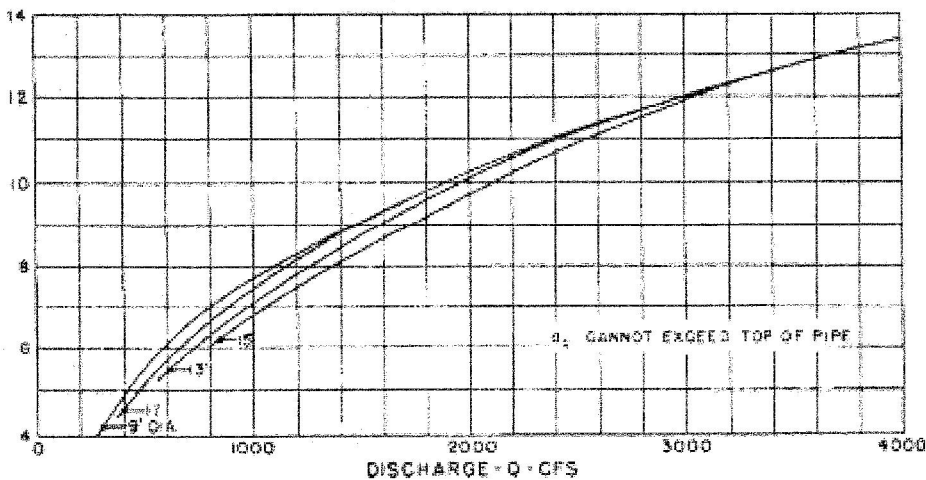
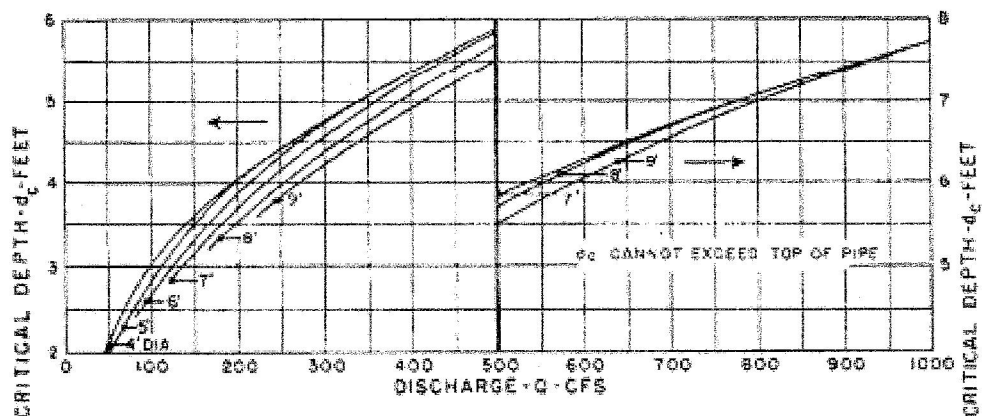
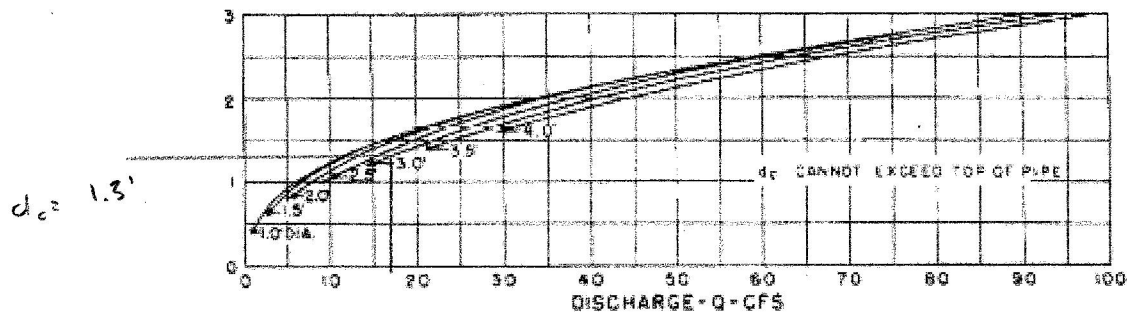
HEAD FOR
STANDARD
C. M. PIPE CULVERTS
FLOWING FULL
 $n = 0.024$

BUREAU OF PUBLIC ROADS JAN. 1953

CRITICAL DEPTH, CIRCULAR PIPE



CHART 4

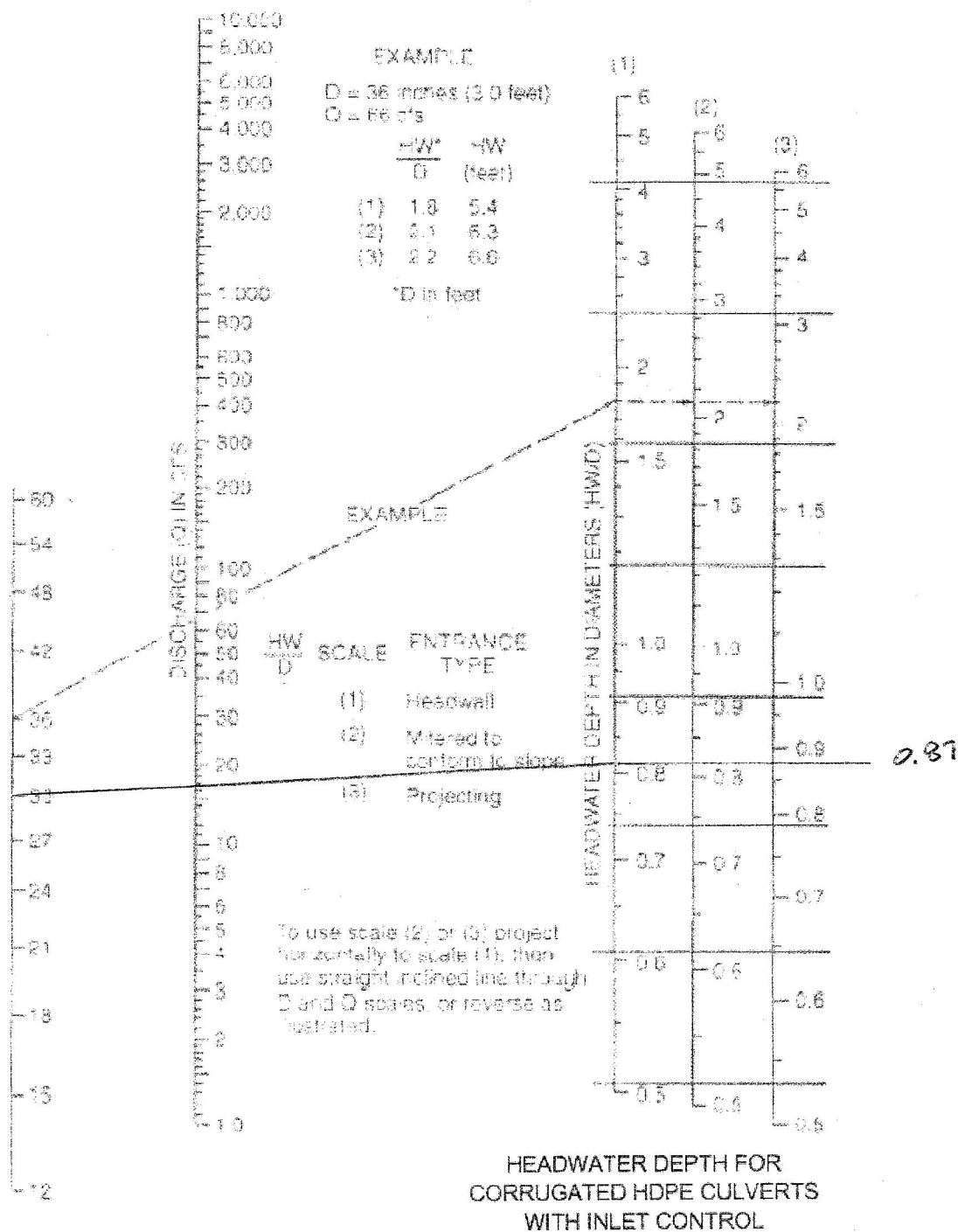


BUREAU OF PUBLIC ROADS

JAN. 1964

CRITICAL DEPTH
CIRCULAR PIPE

INLET CONTROL, CIRCULAR HDPE PIPE



Hydrograph Plot

English

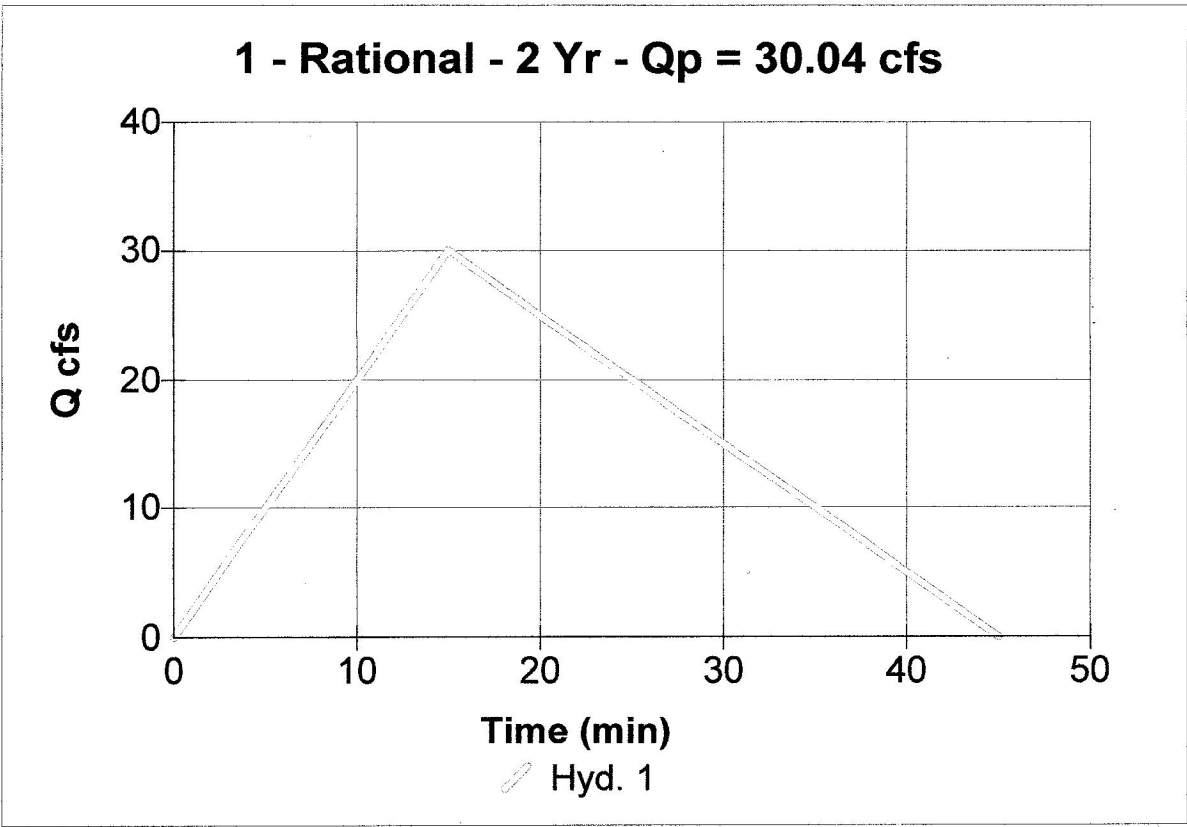
Hyd. No. 1

2 YEAR STORM AT BMP

Hydrograph type = Rational
Storm frequency = 2 yrs
Drainage area = 8.5 ac
Intensity = 3.91 in
I-D-F Curve = NORFOLK1.IDF

Peak discharge = 30.04 cfs
Time interval = 1 min
Runoff coeff. = 0.9
Time of conc. (Tc) = 15 min
Reced. limb factor = 2

Total Volume = 40,561 cuft



Performance Database (NPRPD). In addition, we have liberally borrowed from the cutting-edge ideas expressed in the newer BMP stds & specs from other states in the region.

To assist in development of these BMP stds & specs, a literature search was performed to compile data to support updated runoff volume reduction and pollution removal capabilities for different BMPs. Based on the research findings, runoff volume reduction rates were assigned and removal rates for Total Phosphorus were updated for various BMPs, as shown in **Table 4.1**. The explanation for these decisions can be found in the Technical Memorandum: The Runoff Reduction Method [pdf] developed for DCR and others by the Center for Watershed Protection, in support of DCR's regulation and Handbook revision processes.


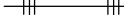













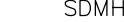





















Table 4.1. BMP Pollutant Removal Efficiencies (March 1, 2011)

Practice Number	Practice	Removal of TP by Runoff Reduction (RR, as %) (based upon 1 inch of rainfall)	Removal of TP by Treatment – Pollutant (EMC) Reduction (PR, as %)	Total Mass Load Removal of Total Phosphorus (TR, as %)
1	Rooftop Disconnection	25 or 50 ¹	0	25 or 50 ¹
2	Sheetflow to Vegetated Filter or Conserved Open Space 1	25 to 50 ¹	0	25 to 50 ¹
	Sheetflow to Vegetated Filter or Conserved Open Space 2 ⁵	50 to 75 ¹	0	50 to 75 ¹
3	Grass Channel	10 to 20 ¹	15	23
4	Soil Amendments	Used to decrease runoff coefficient for turf cover at the site. See the design specs for Roof Disconnection, Sheet Flow to Vegetated Filter or Conserved Open Space, and Grass Channels		
5	Vegetated Roof 1	45	0	45
	Vegetated Roof 2	60	0	60
6	Rainwater Harvesting	Up to 90 ^{3, 5}	0	Up to 90 ^{3, 5}
7	Permeable Pavement 1	45	25	59

	Permeable Pavement	75	25	81
	2			
8	Infiltration 1	50	25	63
	Infiltration 2	90	25	93
9	Bioretention 1	40	25	55
	Bioretention 2	80	50	90
	Urban Bioretention	40	25	55
10	Dry Swale 1	40	20	52
	Dry Swale 2	60	40	76
11	Wet Swale 1	0	20	20
	Wet Swale 2	0	40	40
12	Filtering Practice 1	0	60	60
	Filtering Practice 2	0	65	65
13	Constructed Wetland 1	0	50	50
	Constructed Wetland 2	0	75	75
14	Wet Pond 1	0	50 (45) ⁴	50 (45) ⁴
	Wet Pond 2	0	75 (65) ⁴	75 (65) ⁴
15	Extended Detention Pond 1	0	15	15
	Extended Detention Pond 2	15	15	31

PER PROPERTIES

LEGEND

- | | | | |
|---|----------------------|---|---------------------------|
|  | FIRE HYDRANT |  | OVERHEAD WIRE |
|  | CURB & GUTTER |  | LIGHT POLE |
|  | EDGE OF PAVEMENT |  | POWER POLE |
|  | SWALE |  | CATCH BASIN |
|  | CTV BOX |  | SANITARY SEWER MANHOLE |
|  | SIGN |  | SDMH |
|  | STREET LAMP |  | INVERT |
|  | TELE. BOX |  | GRADE TO DRAIN |
|  | SEWER CLEAN OUT |  | FINISHED GRADE |
|  | WATER METER |  | FLOW LINE |
|  | WATER VALVE |  | TC |
|  | FENCE |  | FIRE HYDRANT |
|  | MANHOLE |  | PROP. ELEVATION |
|  | CATCH BASIN |  | PROP. CONTOUR |
|  | PROPOSED DROP INLET |  | EXIST. ELEVATION |
|  | PROPOSED STORM SEWER |  | VEGETATED WETLANDS |
|  | SEWER PIPE |  | TEMPORARY BENCHMARK (TBM) |
|  | WATER LINE |  | FLARED END SECTION |
| | |  | IRON ROD FOUND |

THIS PLAN DOES NOT GUARANTEE THE EXISTENCE OR LOCATION OF THE UNDERGROUND UTILITIES SHOWN HEREON, NOR DOES IT GUARANTEE THE NON-EXISTENCE OF UNDERGROUND UTILITIES WHICH MAY BE PRESENT. THIS PLAN DOES NOT GUARANTEE THE ABSENCE OF CONFLICTS WITH UNDERGROUND UTILITIES. IF, DURING THE COURSE OF CONSTRUCTION, DISCREPANCIES ARE DISCOVERED BETWEEN THE UNDERGROUND UTILITIES SHOWN ON THIS PLAN AND ACTUAL FIELD CONDITIONS, THE CONTRACTOR SHALL NOTIFY GALLUP SURVEYORS & ENGINEERS, LTD. BEFORE PROCEEDING WITH FURTHER CONSTRUCTION.

IT SHALL BE THE OWNER'S/DEVELOPER'S RESPONSIBILITY TO ASCERTAIN THE EXISTENCE AND/OR NON-EXISTENCE OF THE FOLLOWING WITH REGARDS TO THIS SITE.

- 1) DEED RESTRICTIONS
- 2) JURISDICTIONAL WETLANDS
- 3) HAZARDOUS MATERIALS

PREPARED FOR:

PER PROPERTIES
P.O. BOX 57008
VIRGINIA BEACH, VA. 23457
PHONE: 757-426-6824
FAX: 757-721-9071
ATTN: JIM SALMONS

PREPARED BY:

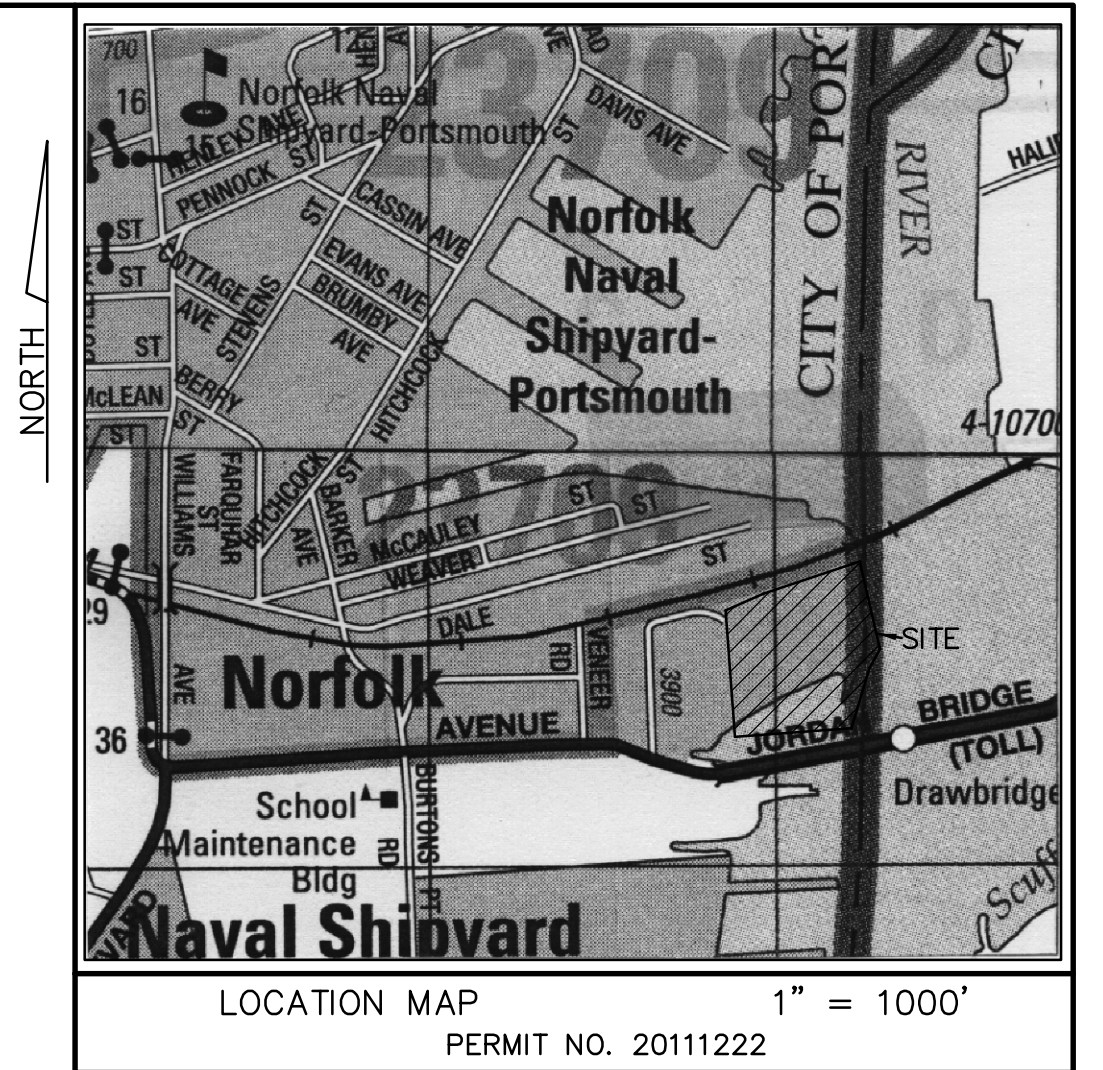
GALLUP SURVEYORS & ENGINEERS, LTD.
323 FIRST COLONIAL ROAD
VIRGINIA BEACH, VIRGINIA 23454
PHONE: 757-428-8132
FAX: 757-425-2390

CONSULTANTS

BOUNDARY SURVEY PREPARED BY STEVE BOONE AND ASSOCIATES, P.C., RECORDED IN M.B. 22, P. 109, 110

CONTAINMENT BERM SHOWN OBTAINED FROM PLANS TITLED, "REMEDIATION DESIGN - PHASE 2, EAST SIDE CONTAINMENT BERM, ATLANTIC WOOD INDUSTRIES SUPERFUND SITE, PREPARED BY EA ENGINEERING, SCIENCE, AND TECHNOLOGY, DATED 1/2011

UTILITIES SHOWN OBTAINED FROM PLANS TITLED, "REMEDIATION DESIGN - PHASE 2, EAST SIDE CONTAINMENT BERM, ATLANTIC WOOD INDUSTRIES SUPERFUND SITE, PREPARED BY EA ENGINEERING, SCIENCE, AND TECHNOLOGY, DATED 1/2011, AND FROM FIELD SURVEY BY GALLUP SURVEYORS AND ASSOCIATES, AND FROM CITY RECORD DRAWINGS.



CONSTRUCTION SEQUENCE

1. OBTAIN ALL REQUIRED PERMITS
2. INSTALL SILT FENCE
3. INSTALL CONSTRUCTION ENTRANCE
4. ADJUST SILT FENCE AS REQUIRED
5. PLACE CRUSHED CONCRETE FILL MATERIAL IN 6" LIFTS
6. EXCAVATE FOR BMP AND STORM DRAINS
7. INSTALL FILTER FABRIC, PIPES, INLETS, AND 57 STONE
8. CONTINUE FILLING AND ADJUSTING BERM
10. INSTALL INLET PROTECTION AS INLETS ARE SET.

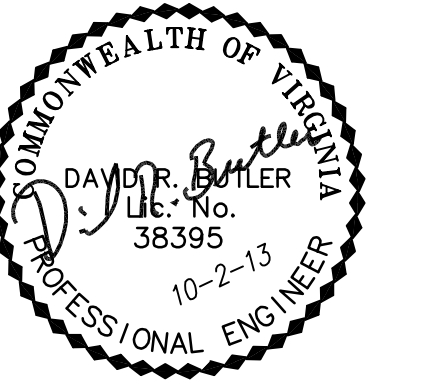
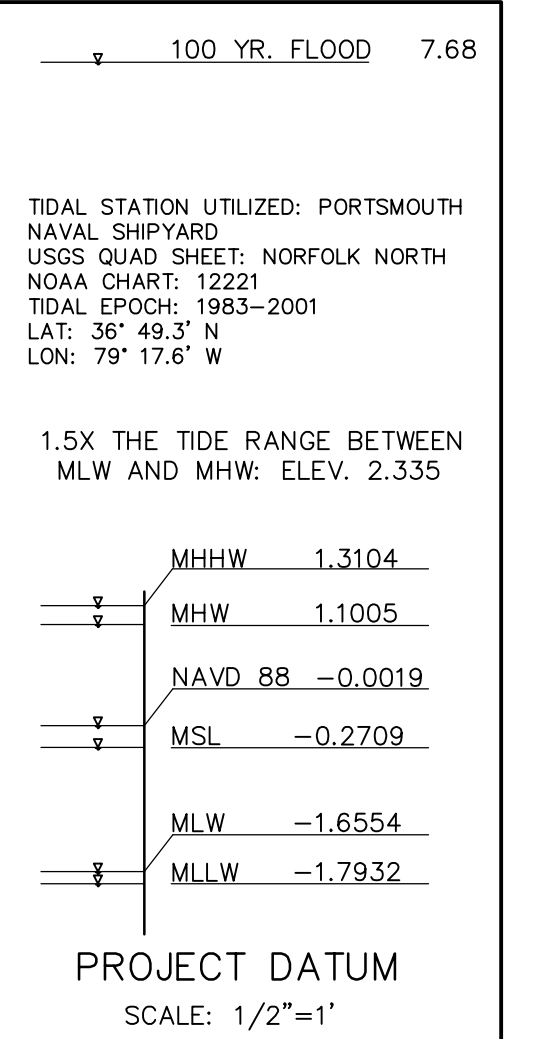
ANY AND ALL MATERIAL/DEBRIS TRACKED ONTO A PUBLIC ROAD SURFACE SHALL BE CLEANED THOROUGHLY AT THE END OF EACH DAY. SEDIMENT SHALL BE REMOVED FROM ROADS BY SHOVELING AND/OR SWEEPING AND BE TRANSPORTED TO A SEDIMENT CONTROLLED DISPOSAL AREA.

ALL CRACKED CONCRETE IN THE R/W SHALL BE REMOVED AND REPLACED TO THE NEAREST JOINT. PATCHING IS NOT ACCEPTABLE.

THE SITE CONTRACTOR SHALL HAVE A RESPONSIBLE
LAND DISTURBER (RLD) CERTIFICATION.

ALL EXCAVATED MATERIAL FROM CONSTRUCTION
SHALL BE DISPOSED OF IN A LAWFUL MANNER.

ALL DISTURBED AREAS SHALL BE
SEEDED. (SEE SCHEDULE)



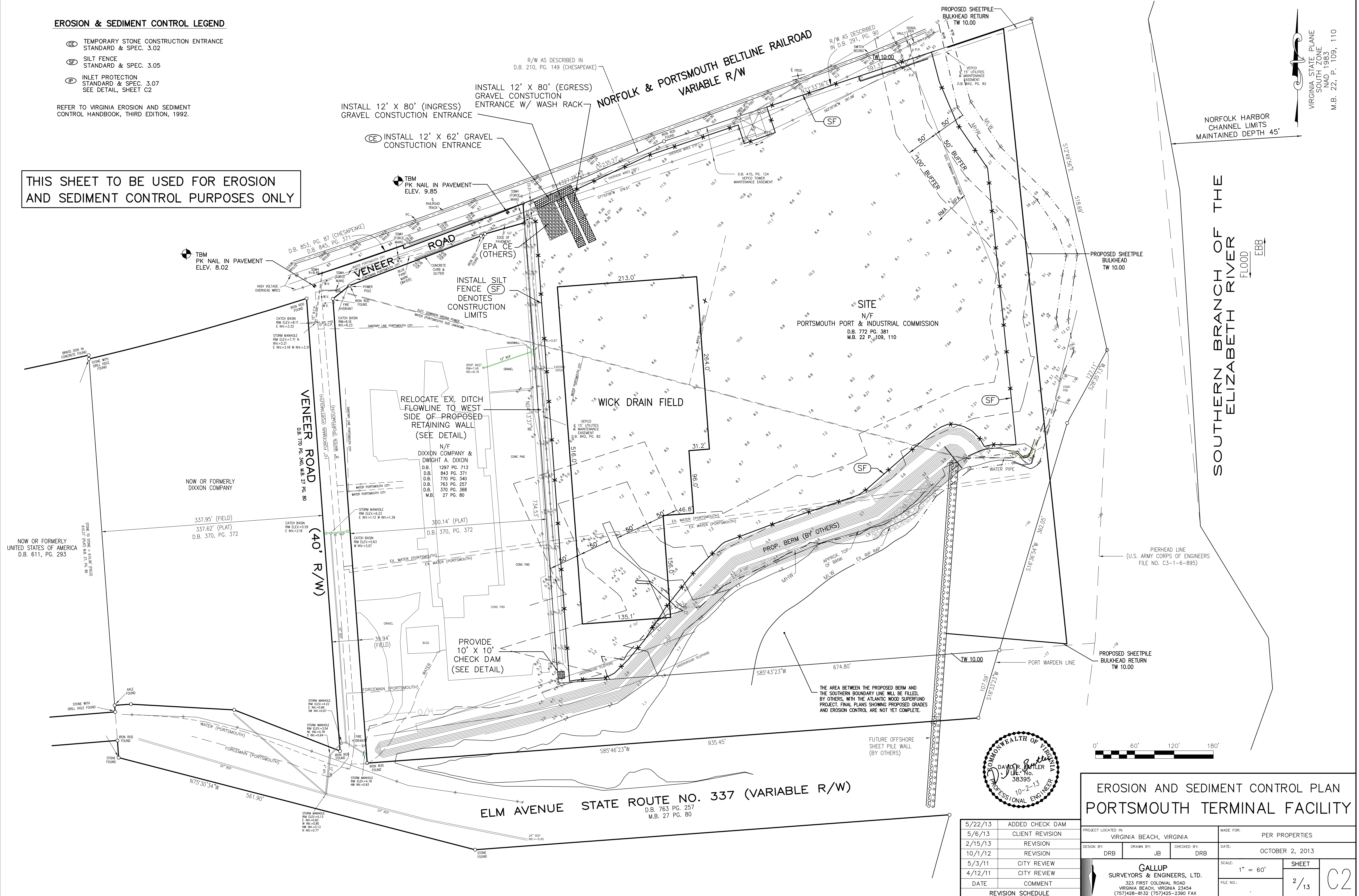
DATE	REVISION

EROSION & SEDIMENT CONTROL LEGEND

- (CE) TEMPORARY STONE CONSTRUCTION ENTRANCE
STANDARD & SPEC. 3.02
- (SF) SILT FENCE
STANDARD & SPEC. 3.05
- (IP) INLET PROTECTION
STANDARD & SPEC. 3.07
SEE DETAIL, SHEET C2

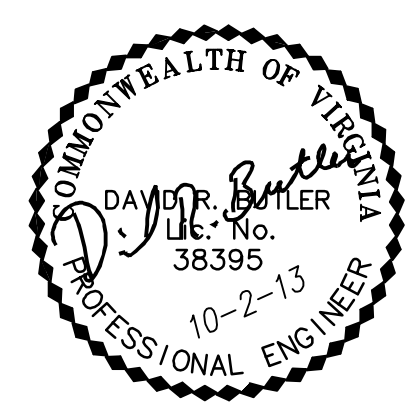
REFER TO VIRGINIA EROSION AND SEDIMENT
CONTROL HANDBOOK, THIRD EDITION, 1992.

THIS SHEET TO BE USED FOR EROSION
AND SEDIMENT CONTROL PURPOSES ONLY



SOUTHERN BRANCH OF THE
ELIZABETH RIVER

VIRGINIA STATE PLANE
SOUTH ZONE
NAD 1983
M.B. 22, P. 109, 110



EROSION AND SEDIMENT CONTROL PLAN PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE: OCTOBER 2, 2013
CALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 60'	SHEET 2/13
REVISION SCHEDULE		C2	

5/22/13	ADDED CHECK DAM
5/6/13	CLIENT REVISION
2/15/13	REVISION
10/1/12	REVISION
5/3/11	CITY REVIEW
4/12/11	CITY REVIEW
DATE	COMMENT

DRAINAGE STRUCTURE SCHEDULE

1A. STMH RIM 10.50 INV 4.37	8. STMH RIM 10.50 INV -1.05	10-10A 208'-24" HDPE @ 0.25% INV IN 4.77, INV OUT 4.25
1. STMH RIM 10.50 INV 4.24	10. DI RIM 9.80 INV 4.77	10A-11 207'-24" HDPE @ 0.25% INV IN 4.25, INV OUT 3.73
2. STMH RIM 10.50 INV 4.04	11. DI RIM 9.80 INV 3.73	11-12 199'-24" HDPE @ 0.20% INV IN 3.73, INV OUT 3.33
3. STMH RIM 10.50 INV 3.73	12. STMH RIM 10.40 INV 3.33	12-12A 59'-24" HDPE @ 0.34% INV IN 3.33, INV OUT 3.13
4. STMH RIM 8.20 INV (N) 3.51 INV (E) -0.14 INV (W) 2.50	12A. DI RIM 9.50 INV 3.13	12A-13 191'-24" HDPE @ 0.34% INV IN 3.13, INV OUT 2.49
5. STMH RIM 10.20 INV -0.37	13. DI RIM 9.35 INV 2.49 (E,W,S) INV 7.29 (N)	RR-13 117'-12" HDPE @ 1.03% INV IN 8.50, INV OUT 7.29
6. DI RIM 9.40 INV (E) -0.58 INV (W) 1.87 INV (S) 3.41	14. DI RIM 9.35 INV 2.96	9A-8A 109'-18" PERFORATED HDPE @ 0.60% INV IN 4.09, INV OUT 3.44
7. STMH RIM 10.50 INV -0.86	15. DI RIM 9.35 INV 3.23	15-14 89'-18" HDPE @ 0.30% INV IN 3.23, INV OUT 2.96
5A. DI RIM 9.10 INV 5.09	7A. DI RIM 9.50 INV (N,S) 2.00 INV (E) 4.00	
10A. DI RIM 9.80 INV 4.25	8A. RIM 9.60 INV 3.44	
	9A. RIM 9.35 INV 4.09	
	6A. RIM 9.80 INV -0.57	

NOTES:
THE SILT SACK PRODUCT SHOWN ON SHEET C7 IS TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN PERMANENT FOR DRAINAGE STRUCTURES 7A, 8A, 9A, AND 13.

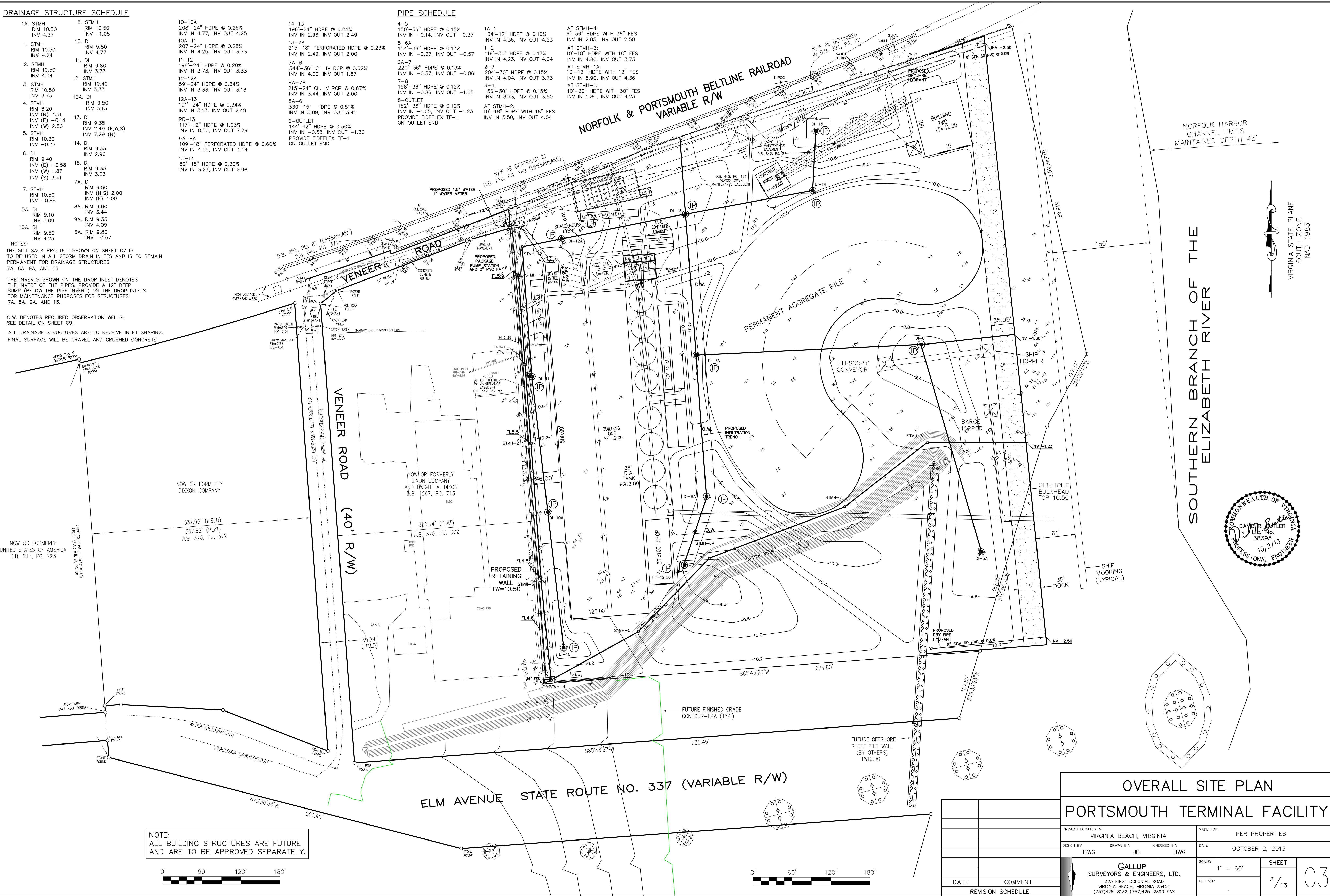
THE INVERTS SHOWN ON THE DROP INLET DENOTES THE INVERT OF THE PIPES. PROVIDE A 12" DEEP SUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS FOR MAINTENANCE PURPOSES FOR STRUCTURES 7A, 8A, 9A, AND 13.

O.W. DENOTES REQUIRED OBSERVATION WELLS; SEE DETAIL ON SHEET C9.

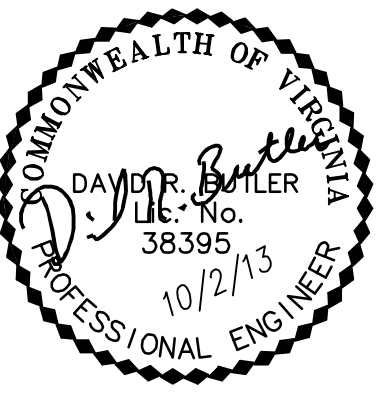
ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING. FINAL SURFACE WILL BE GRAVEL AND CRUSHED CONCRETE.

PIPE SCHEDULE

4-5 150'-36" HDPE @ 0.15% INV IN -0.14, INV OUT -0.37	1A-1 134'-12" HDPE @ 0.10% INV IN 4.36, INV OUT 4.23	AT STMH-4: 6'-36" HDPE WITH 36" FES INV IN 2.85, INV OUT 2.50
5-6A 154'-36" HDPE @ 0.13% INV IN -0.37, INV OUT -0.57	1-2 119'-30" HDPE @ 0.17% INV IN 4.23, INV OUT 4.04	AT STMH-3: 10'-18" HDPE WITH 18" FES INV IN 4.80, INV OUT 3.73
6A-7 220'-36" HDPE @ 0.13% INV IN -0.57, INV OUT -0.86	2-3 204'-30" HDPE @ 0.15% INV IN 4.04, INV OUT 3.73	AT STMH-1A: 10'-12" HDPE WITH 12" FES INV IN 5.90, INV OUT 4.36
7-8 158'-36" HDPE @ 0.12% INV IN -0.86, INV OUT -1.05	3-4 156'-30" HDPE @ 0.15% INV IN 3.73, INV OUT 3.50	AT STMH-1: 10'-30" HDPE WITH 30" FES INV IN 5.80, INV OUT 4.23
8-OUTLET 152'-36" HDPE @ 0.12% INV IN -1.05, INV OUT -1.23 PROVIDE TIDEFLEX TF-1 ON OUTLET END	AT STMH-2: 10'-18" HDPE WITH 18" FES INV IN 5.50, INV OUT 4.04	

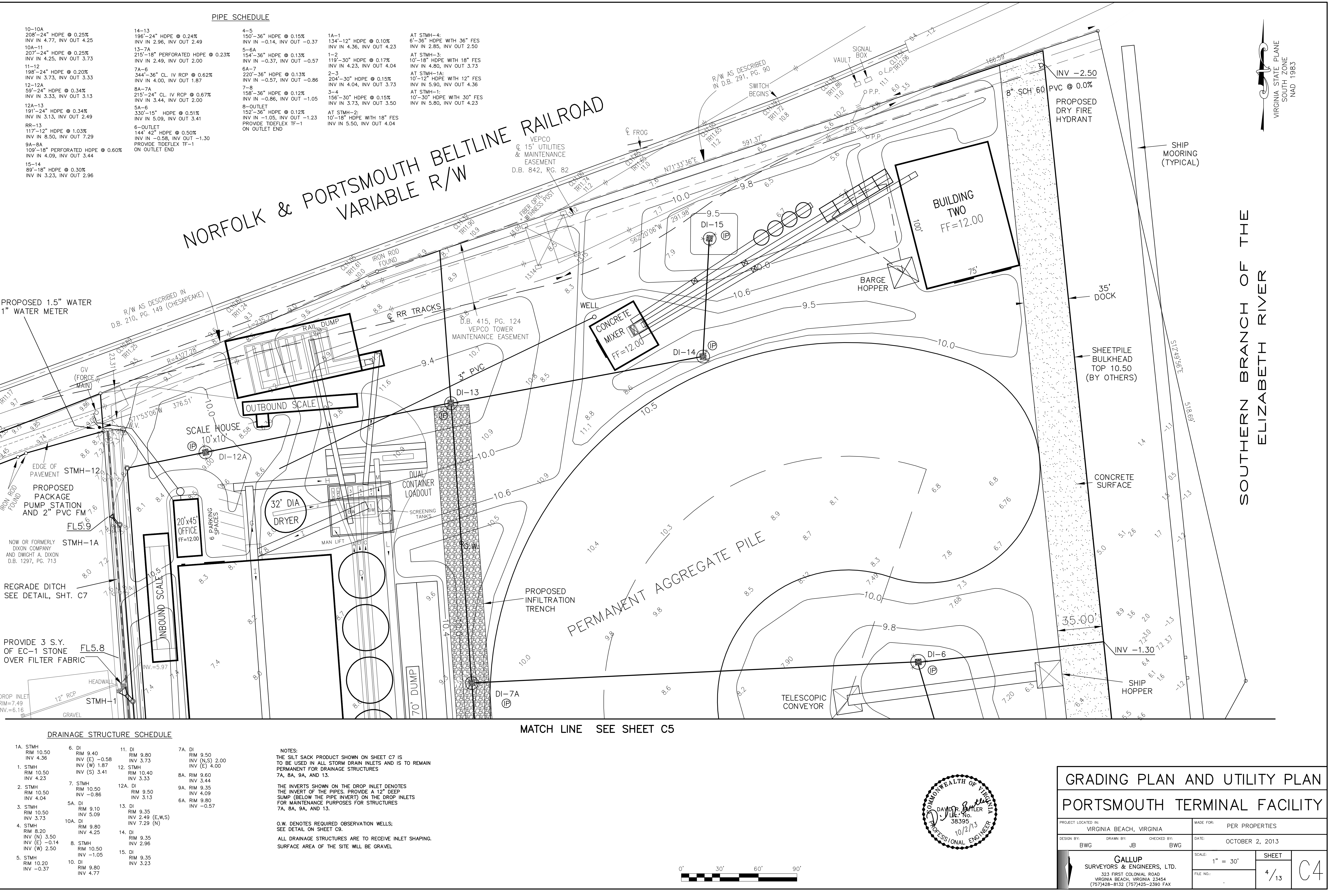


SOUTHERN BRANCH OF THE ELIZABETH RIVER

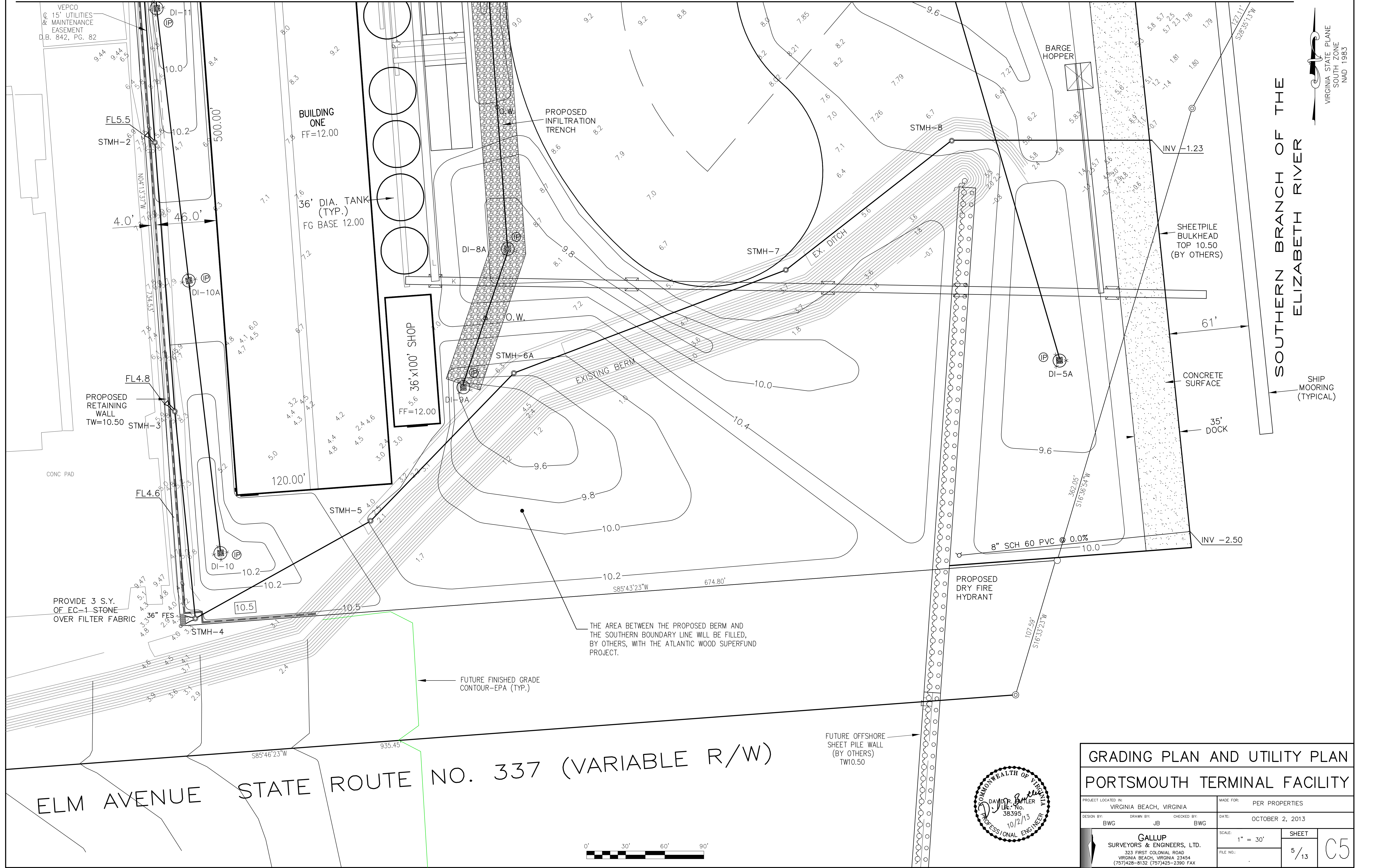


OVERALL SITE PLAN			
PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA	MADE FOR: PER PROPERTIES		
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 60'	SHEET 3 / 13
DATE		COMMENT	
REVISION SCHEDULE			

VIRGINIA STATE PLANE
SOUTH ZONE
NAD 1983



MATCH LINE SEE SHEET C4



VIRGINIA STATE PLANE
SOUTH ZONE
NAD 1983

SOUTHERN BRANCH OF THE
ELIZABETH RIVER

SHIP
MOORING
(TYPICAL)

SHEETPILE
BULKHEAD
TOP 10.50
(BY OTHERS)

CONCRETE
SURFACE

35'
DOCK

INV -2.50

PROPOSED
DRY FIRE
HYDRANT

FUTURE OFFSHORE
SHEET PILE WALL
(BY OTHERS)
TW10.50

THE AREA BETWEEN THE PROPOSED BERM AND
THE SOUTHERN BOUNDARY LINE WILL BE FILLED,
BY OTHERS, WITH THE ATLANTIC WOOD SUPERFUND
PROJECT.

FUTURE FINISHED GRADE
CONTOUR-EPA (TYP.)

PROVIDE 3 S.Y.
OF EC-1 STONE
OVER FILTER FABRIC

CONC PAD

PROPOSED RETAINING
WALL
TW=10.50

BUILDING
ONE
FF=12.00

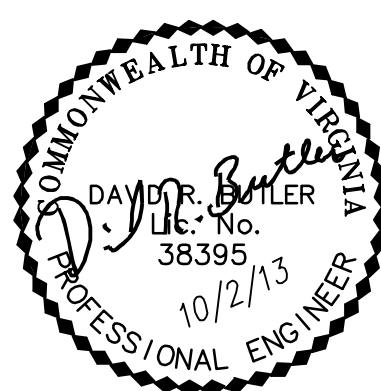
36' DIA. TANK
(TYP.)
FG BASE 12.00

36'x100' SHOP
FF=12.00

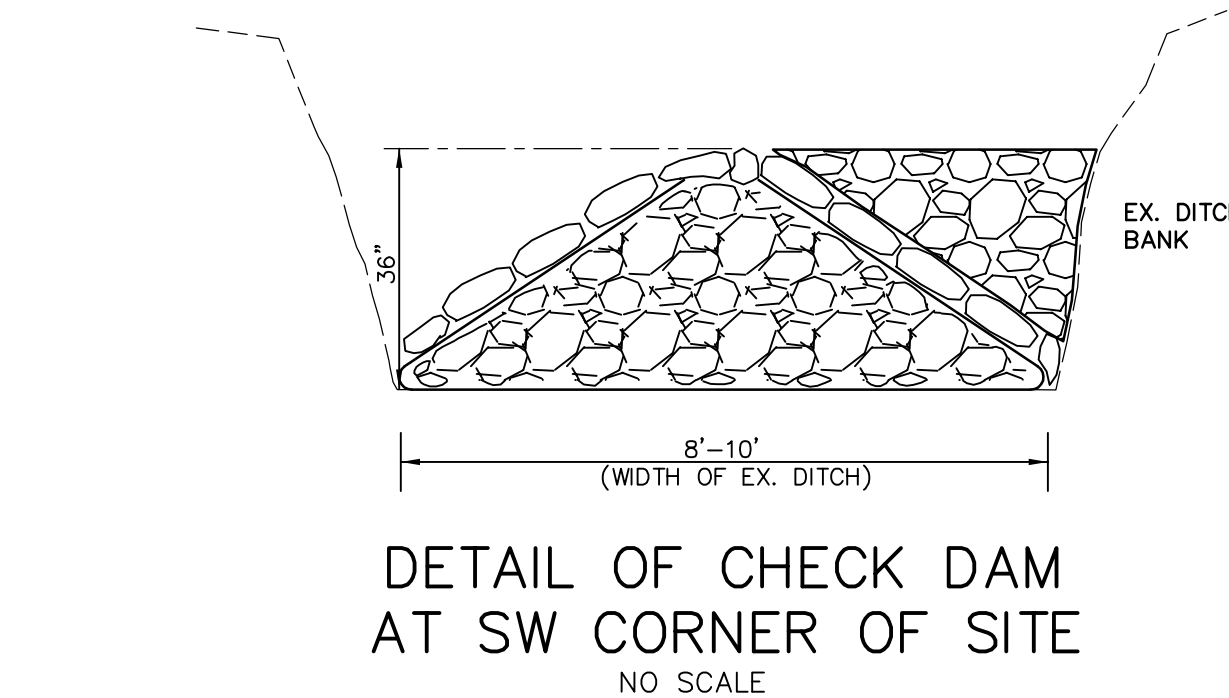
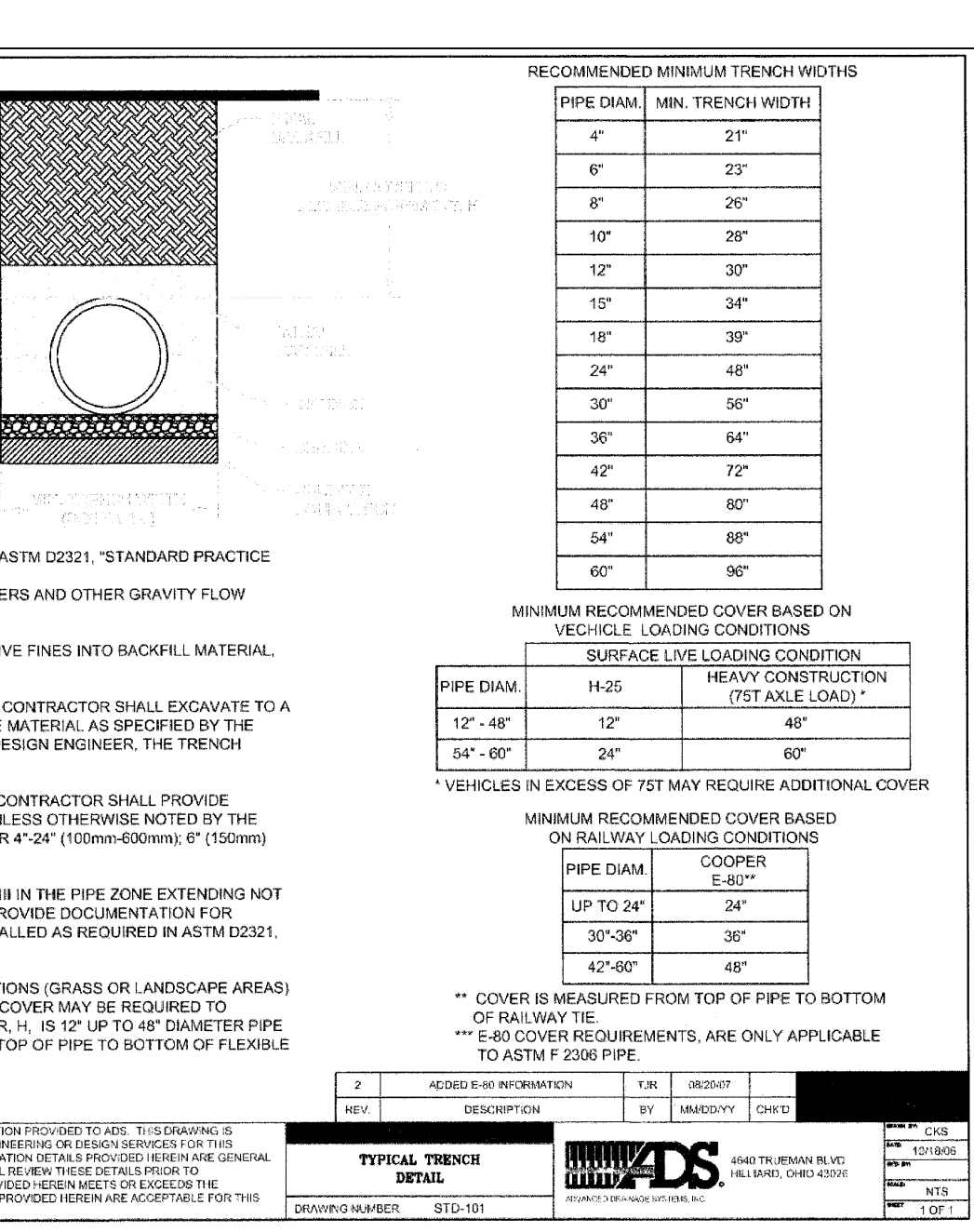
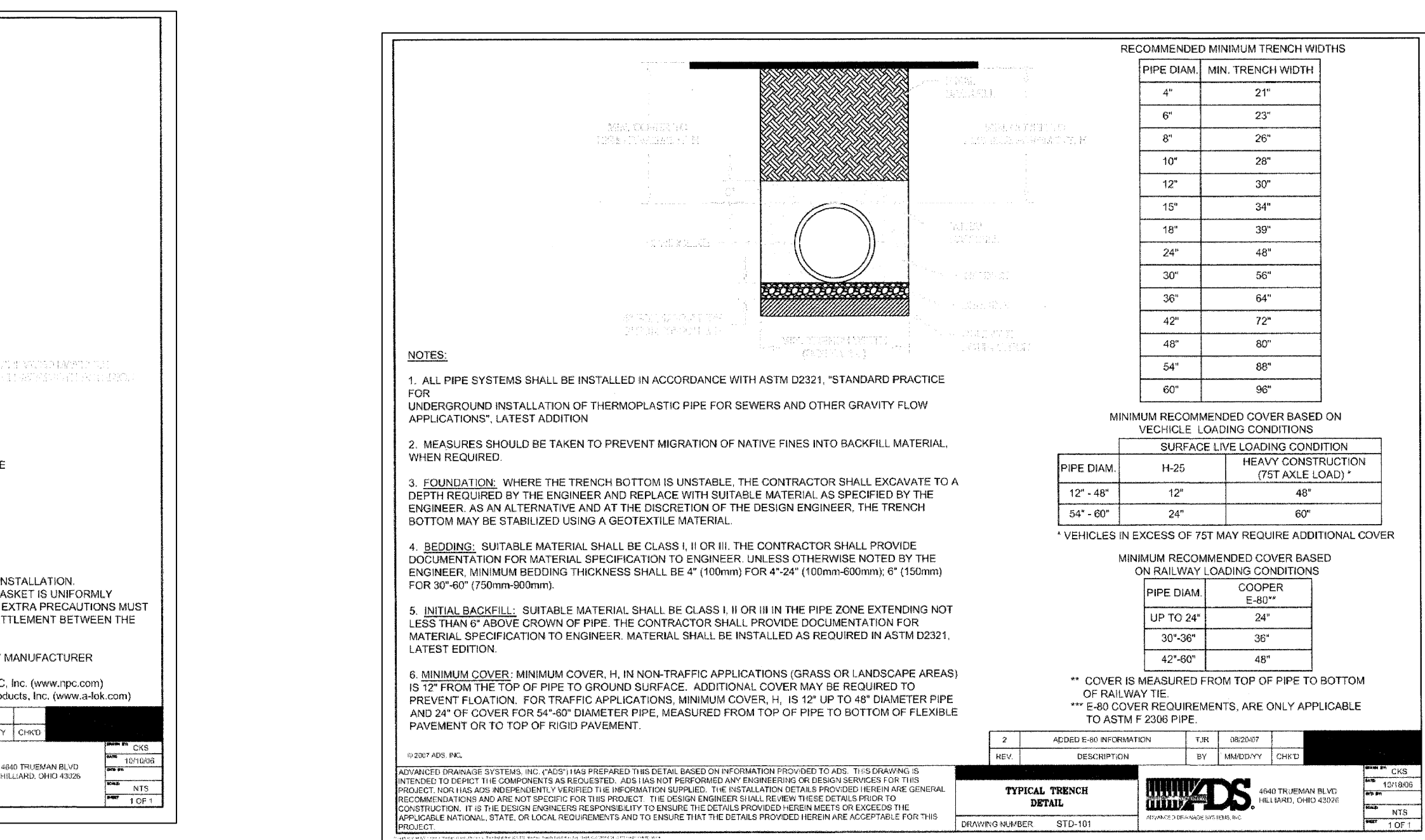
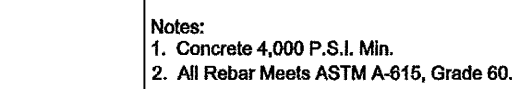
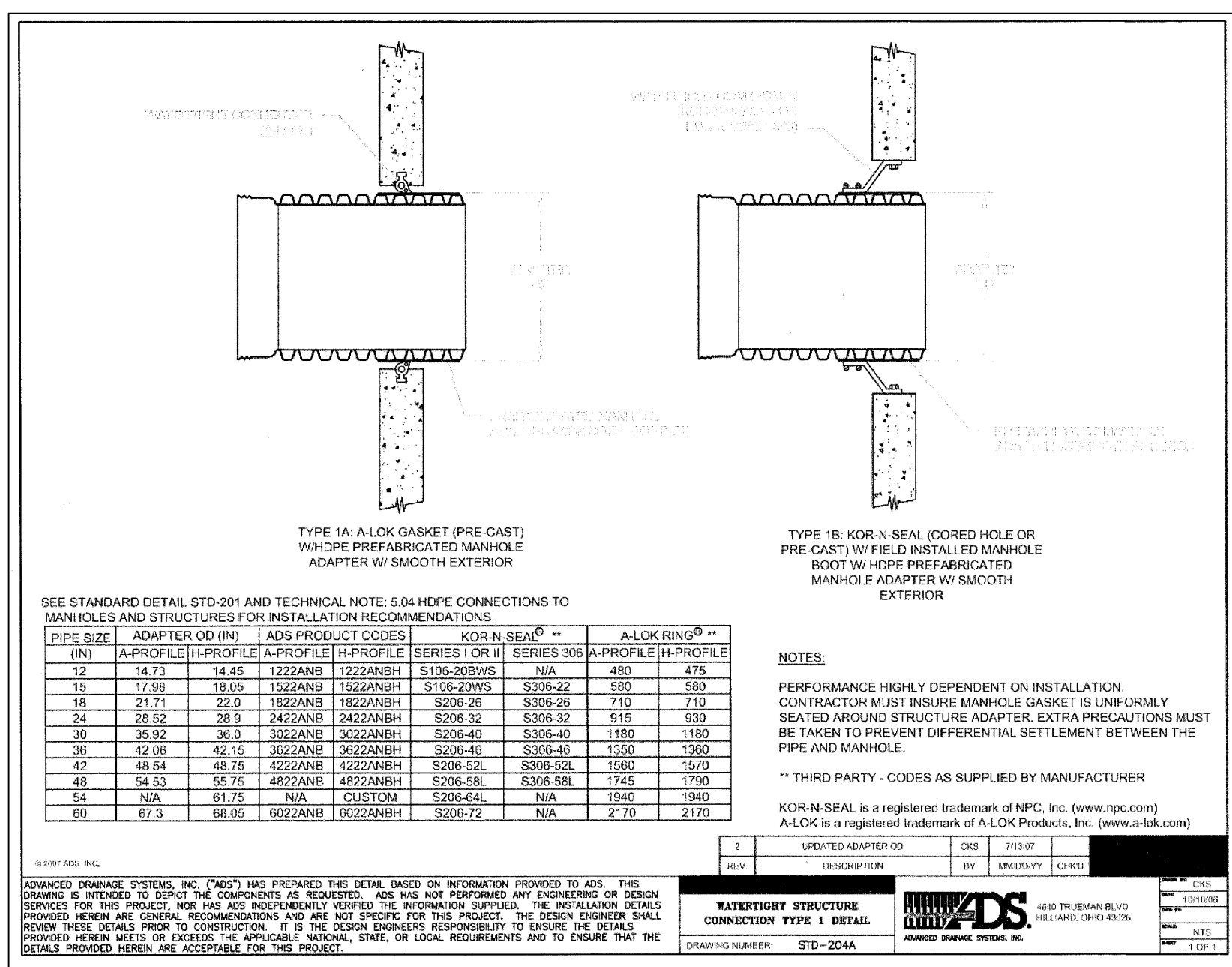
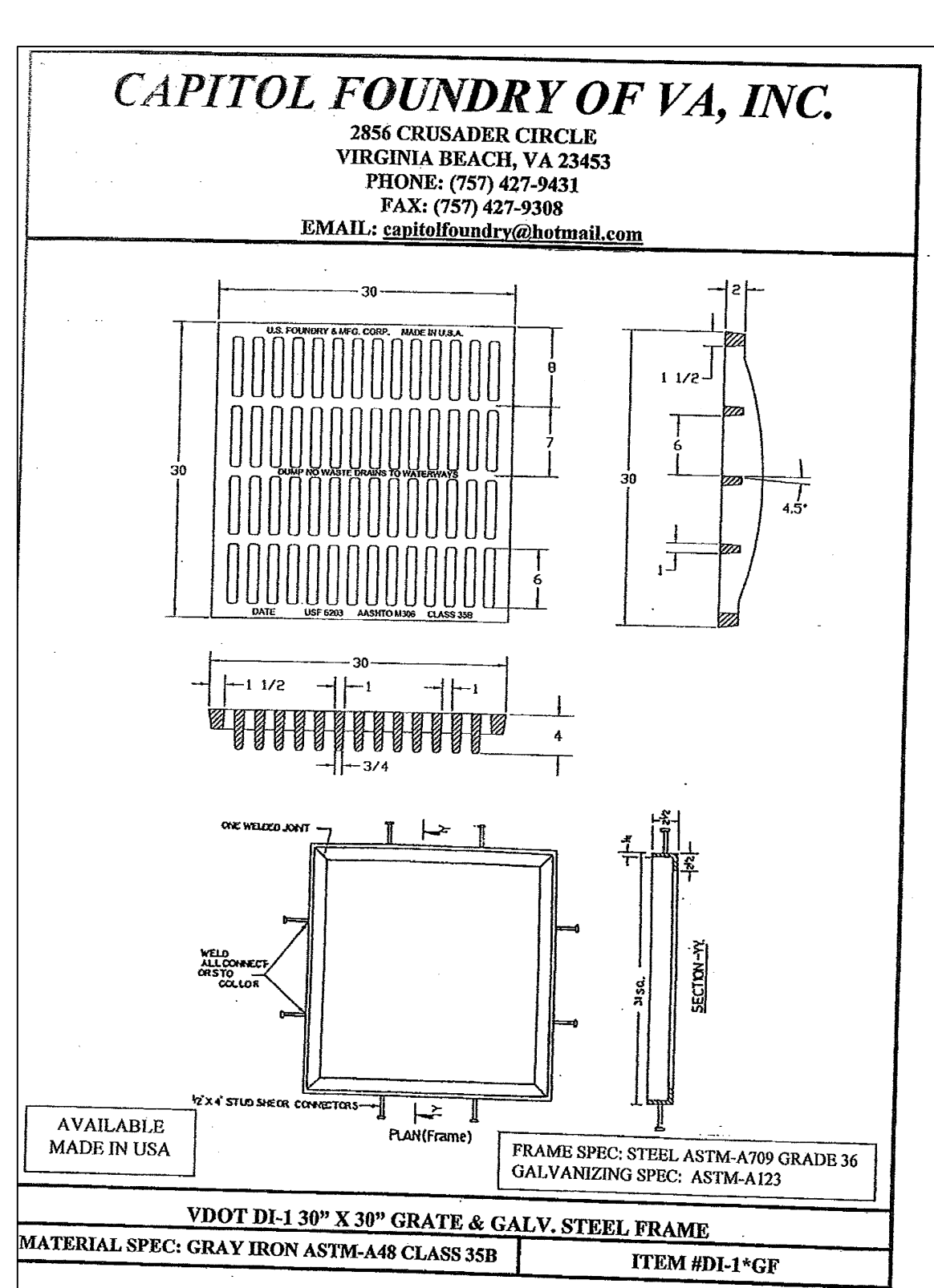
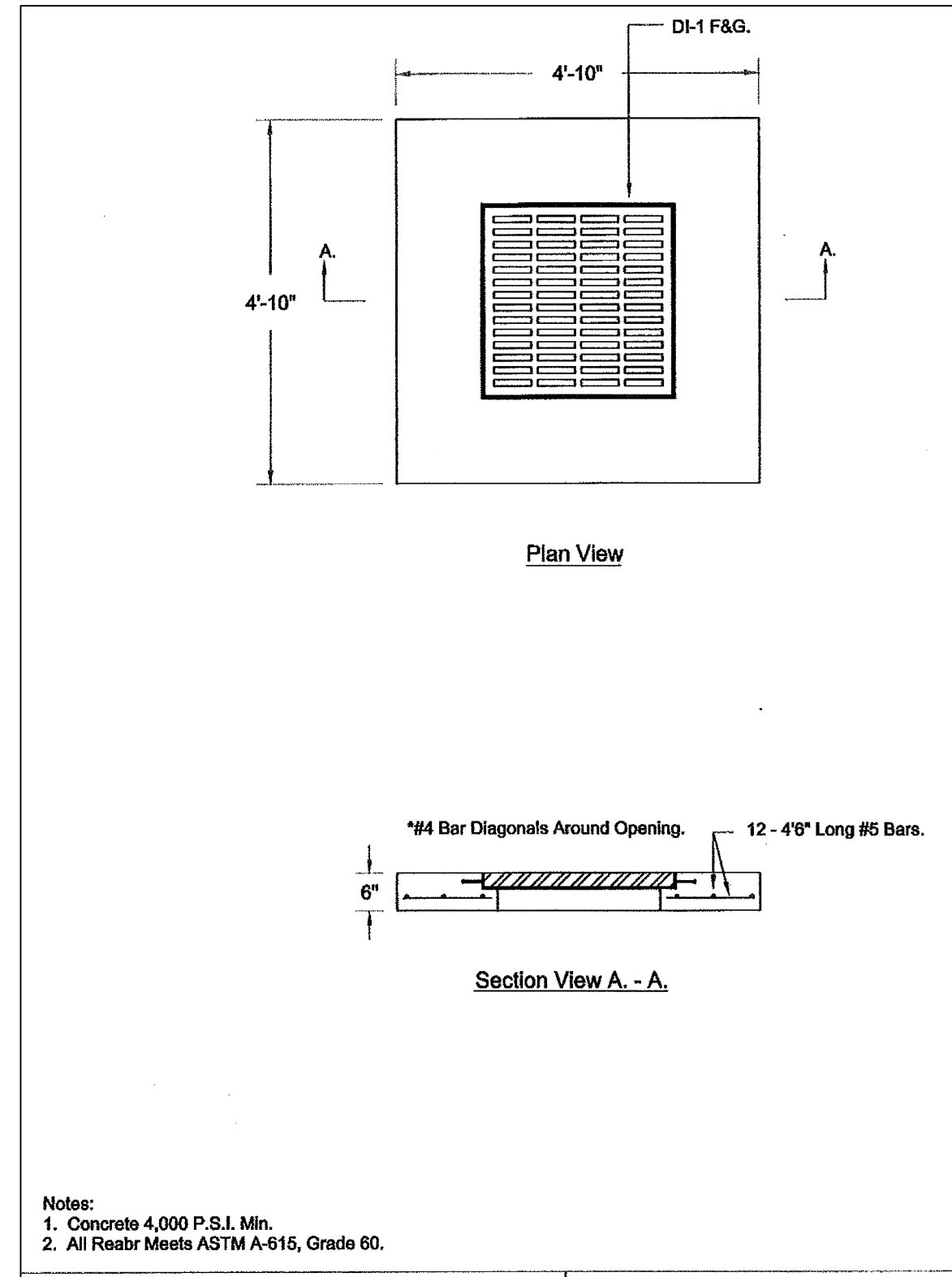
VEPCO
15' UTILITIES
& MAINTENANCE
EASEMENT
D.B. 842, PG. 82

ELM AVENUE

STATE ROUTE NO. 337 (VARIABLE R/W)



GRADING PLAN AND UTILITY PLAN			
PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 30'	SHEET 5/13
		FILE NO.:	C5



Optional Overflow

Insert 1' Rebar For Bag Removal From Inlet (Rebar Not Included)

Silt Sack

Dump Loops (Rebar Not Included)

Expansion Restraint

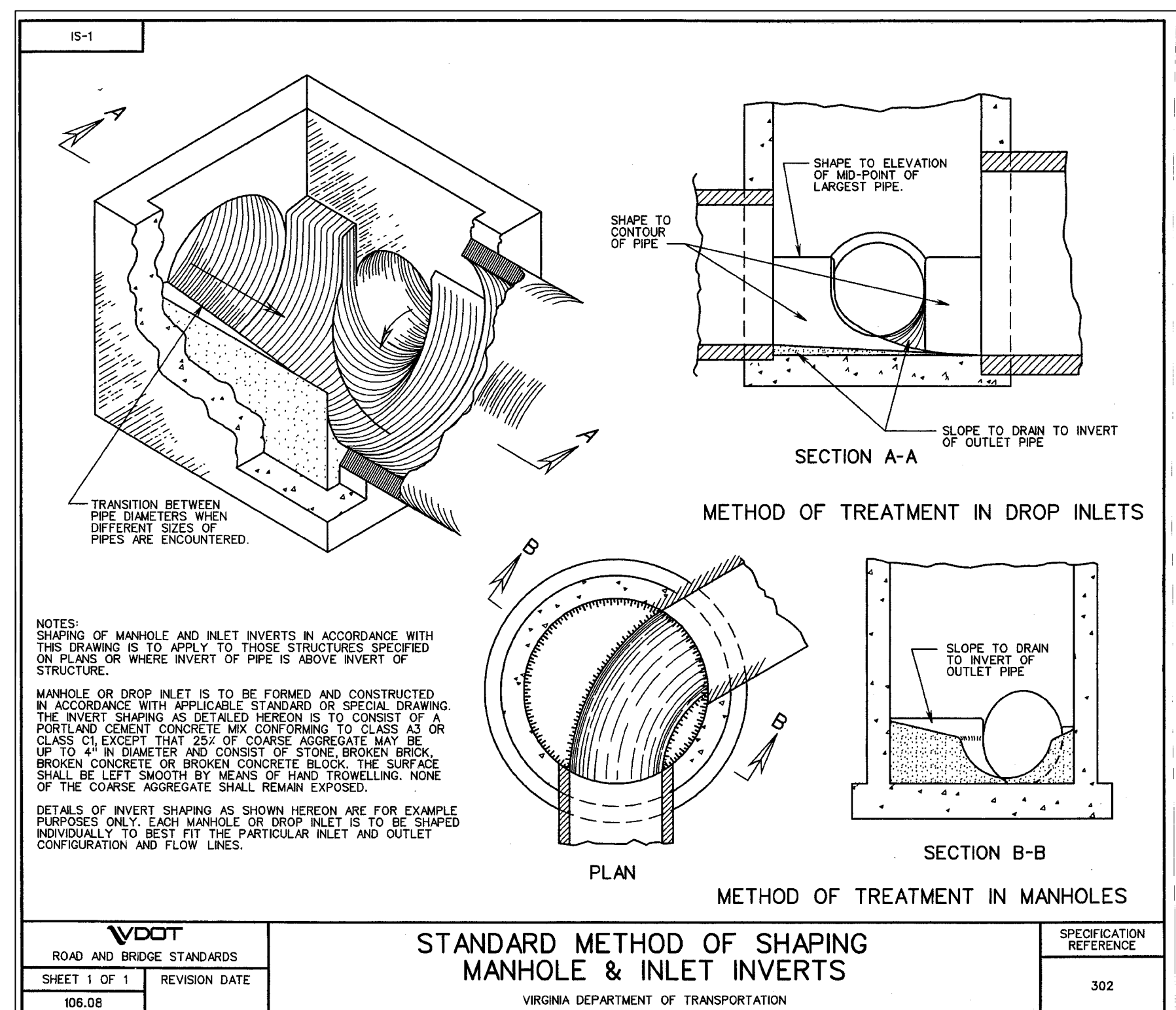
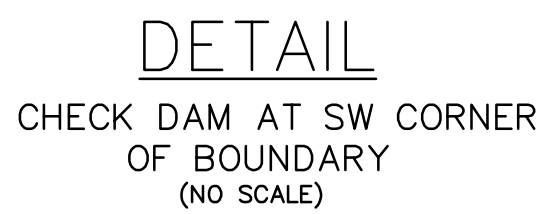
SIZE: 21" X 21" (ADJUSTABLE)
PTH: 18" MIN.

CONFIRM SIZE WITH MANUFACTURER PRIOR TO ORDERING

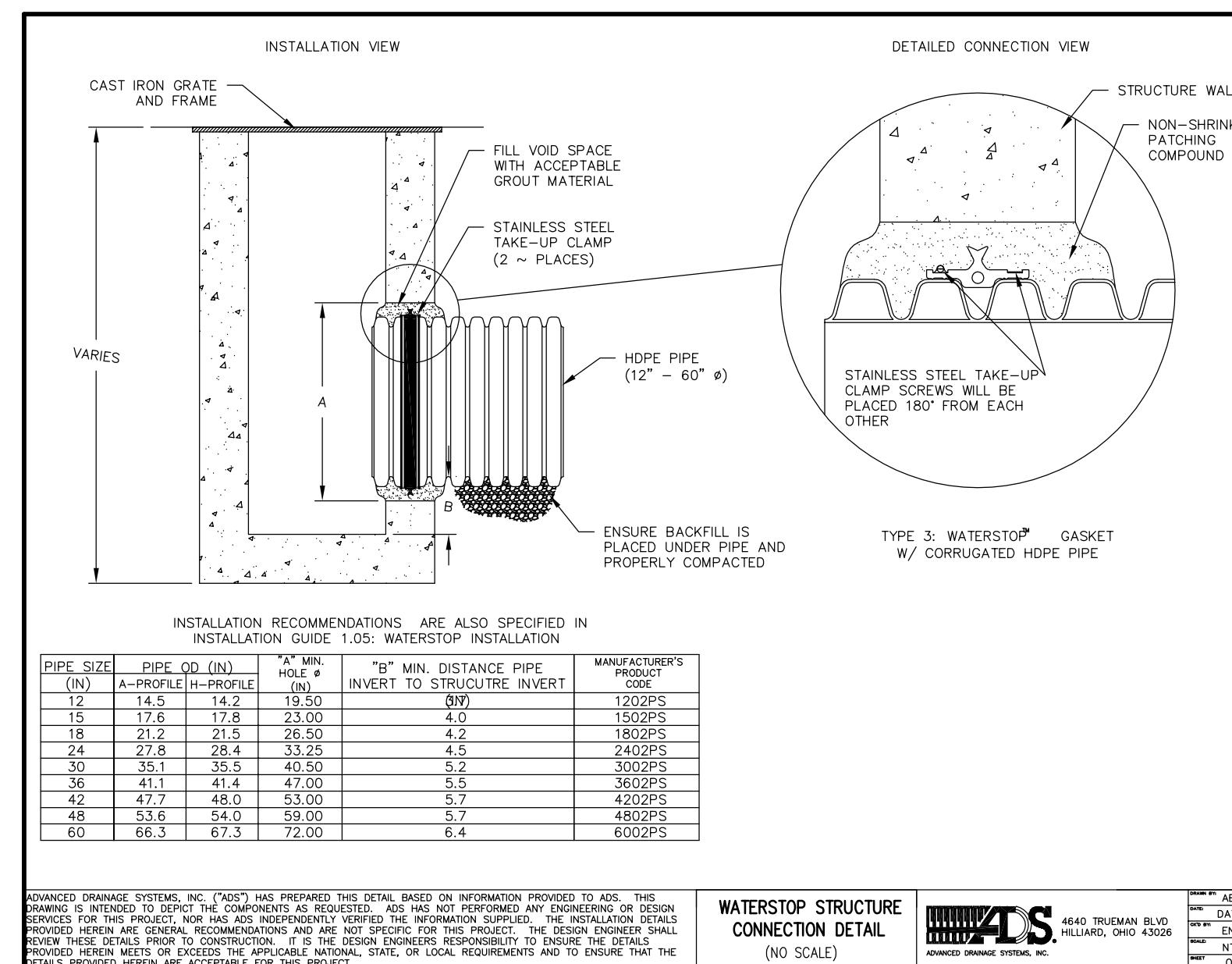
1. EACH SILTSACK SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT
2. IF THERE HAVE BEEN NO MAJOR STORM EVENTS, SILTSACK SHOULD BE INSPECTED EVERY 2-3 WEEKS.
3. THE YELLOW RESTRAINT CORD SHOULD BE VISIBLE AT ALL TIMES. IF THE CORD IS COVERED WITH SEDIMENT, THE SILTSACK SHOULD BE EMPLOYED.

3.0	Construction Sequence
3.1	General
3.1.1	To install Siltsack in the catch basin, remove the grate and place the silt sack in the opening. Hold approximately six inches of the sack outside the frame. This is the area of the lifting straps. Replace the grate to hold the sack in place.
3.1.2	When the restraint cord is no longer visible, Siltsack is full and should be emptied.
3.1.3	To remove Siltsack, take two pieces of 1" diameter rebar and place through the lifting loops on each side of the sack to facilitate the lifting of Siltsack.
3.1.4	To empty Siltsack, place unit where the contents will be collected. Place the rebar through the lift straps (connected to the bottom of the sack) and lift. This will lift Siltsack from the bottom and empty the contents. Clean out and rinse. Return Siltsack to its original shape and place back in the basin.
3.1.5	Siltsack is reusable. Once the construction cycle is complete, remove Siltsack from the basin and clean. Siltsack should be stored out of sunlight until next use.

THE SILT SACK PRODUCT SHOWN ON THIS SHEET
TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN
PERMANENT FOR DRAINAGE STRUCTURES 12-22




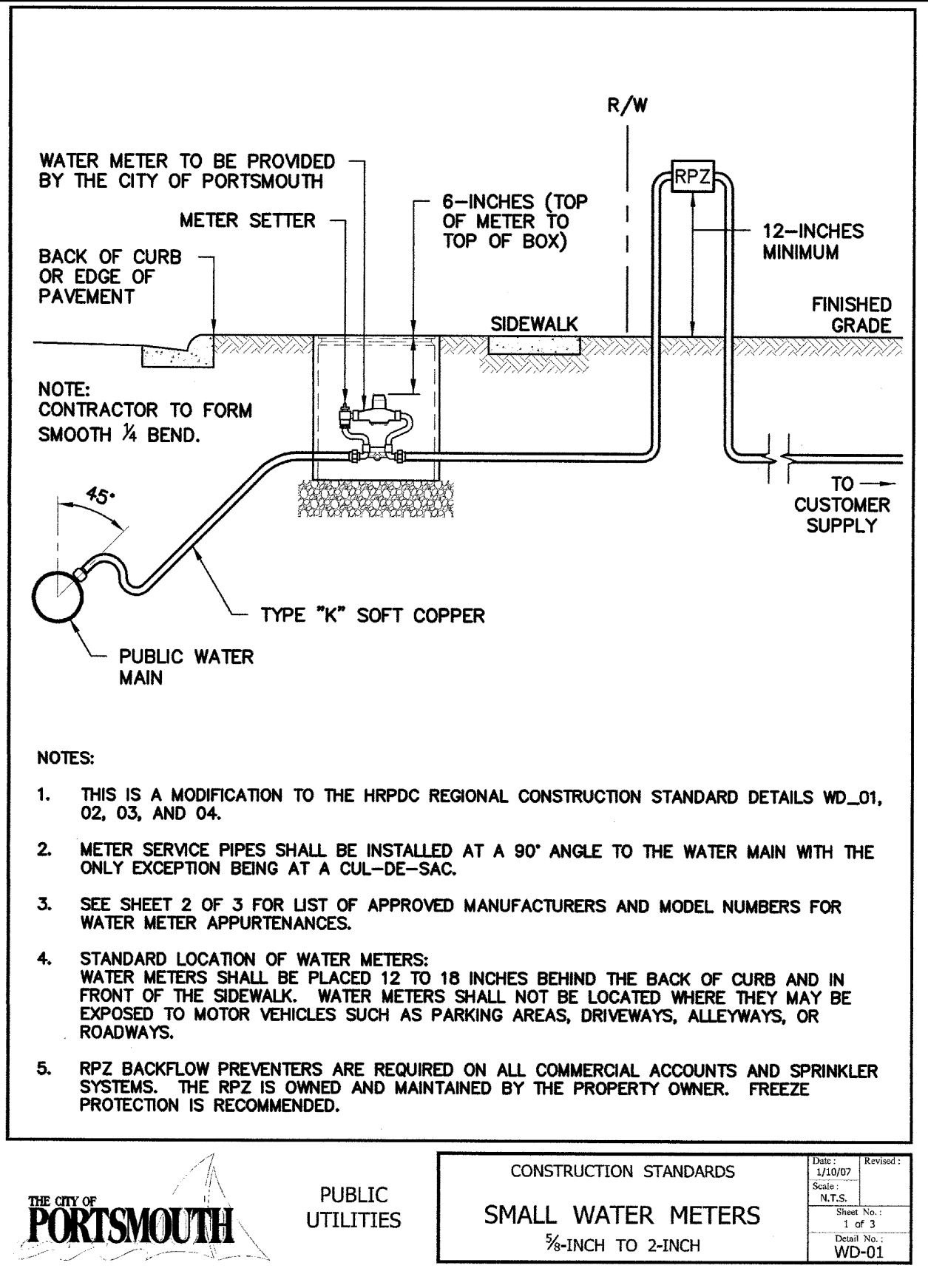
ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET
SHAPING WITH THE EXCEPTION OF STRUCTURES 12-22.



PROJECT LOCATED IN:			MADE FOR:		
VIRGINIA BEACH, VIRGINIA			PER PROPERTIES:		
DESIGN BY:	DRAWN BY:	CHECKED BY:	DATE:		
DRB	JB	DRB	OCTOBER 2, 2013		
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23464 (757)428-8132 (757)425-2390 FAX			SCALE:	SHEET	
			N/A		
			FILE NO.:	9 / 13	

COMMONWEALTH OF VIRGINIA
 DAVID R. BUTLER
 Lic. No.
 38395
 10-2-13
 PROFESSIONAL ENGINEER

		PROJECT LOCATED IN:		MADE FOR:			
		VIRGINIA BEACH, VIRGINIA		PER PROPERTIES			
		DESIGN BY:	DRAWN BY:	CHECKED BY:	DATE:		
		DRB	JB	DRB	OCTOBER 2, 2013		
		 GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX			SCALE:	SHEET	C7
					N/A	9 / 13	
DATE	COMMENT	FILE NO.:					
REVISION SCHEDULE							



METER APPURTENANCES		METER SIZE (in.)			
	%	%	1	1 ½	2
Corporation Stop Criteria	Corporation Stop shall have nominal sized ball valve, AWWA taper thread inlet, and pack joint for type K copper outlet.				
Corporation Size (in.)	%		1	1 ½	2
A.Y. McDonald Ford Mueller	4071B-22 FB1000 P-25008		4071B-22 FB1000 P-25008	4701B-22 FB1000 P-25008	4701B-22 FB1000 P-25008
			Tee Head adapter shall be provided.		
Tapping Criteria for Ductile Iron and Cast Iron Pipe	%	and 1-inch direct tapping.		1 ½ and 2-inch taps shall include a full circle stainless steel clamp. The clamp shall have stainless steel lugs, bolts and nuts, plus a full circle lap gasket.	
Ford Romac Smith-Blair				FS 1 or 2 SS1 264 or 265	FS 1 or 2 SS2 264 or 265
Tapping Criteria for 2-inch HDPE Pipe	%	and 1-inch taps shall include a gasketed bronze saddle with bronze or stainless steel hardware.		1 ½ and 2-inch taps shall not be made on 2-inch HDPE	
Ford Mueller A.Y. McDonald	S70 S-13000		S70 S-13000 3891		
Copper	Nominal size type K copper				
Meter Setter Criteria	Copper setter shall be horizontal with nominal sized ball valve, inlets and outlets. Setter depth shall be 12-inches. Setter shall fit displacement meter.				
Meter Length (in.)	7.5	9	10.75	13	17
Inlet and Outlet Connections	Setter inlet pack joint and outlet pipe thread. Meter inlet and outlet pipe thread.			Setter inlet pack joint and outlet pipe thread. Meter inlet and outlet shall be AWWA flange.	
A.Y. McDonald Ford Mueller	26-112WX2D33 VB-71-12 HP-1578	26-312WX2D33 VB72-44-33 HP-1578	26-412WX2D44 VB74-12W4144 HP-1578	26-612WNFF-66 VBH76-12-11-66 HP-1422-90	26-712-WNFF-77 VBH77-12-77 HP-1422-90
Meter Box Criteria	PVC Box with PVC Cover 20.6-inches x 11.35-inches			PVC Box with Cast Iron Cover 30-inches x 18-inches	
Southeastern Distributors, Inc.	Cover Box	189-Sensus 190		Cover Box	MSBC-1730-R MSBC-1730-18
Carson Industries					
NOTES:					
1. Each 1 ½ or 2-inch meter connection requires full time City inspection.					
2. Service pipeline shall be jointless from corporation stop to meter setter.					
3. Service pipeline size shall only be changed at the inlet to the meter setter, and the changed size is only allowed with a standard brass reducer.					

THE CITY OF

PORTSMOUTH

PUBLIC UTILITIES

SMALL WATER METERS

¾-INCH TO 2-INCH

Sheet No. 11042

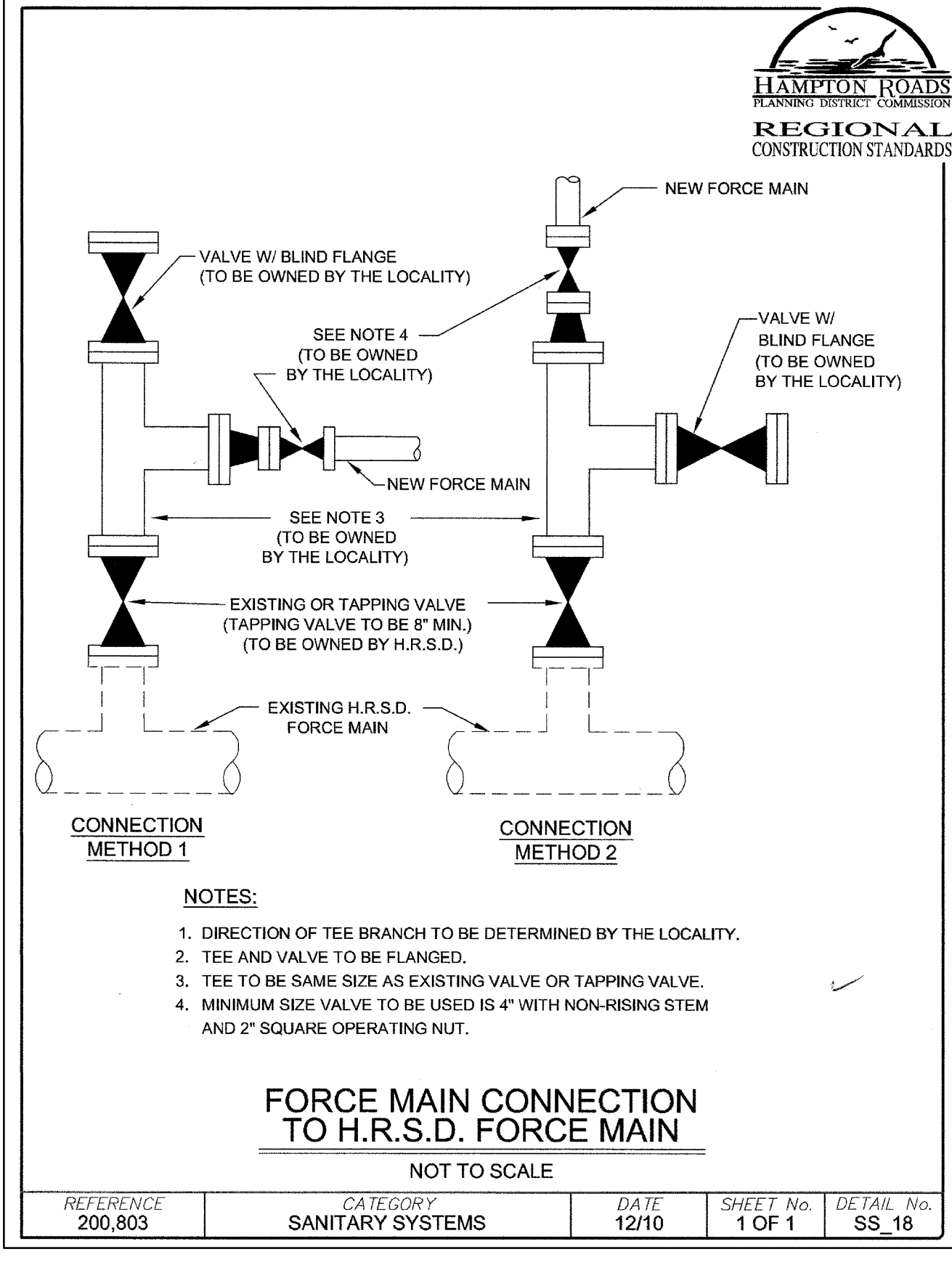
Revision

None

2 of 3

DATE

WD-02



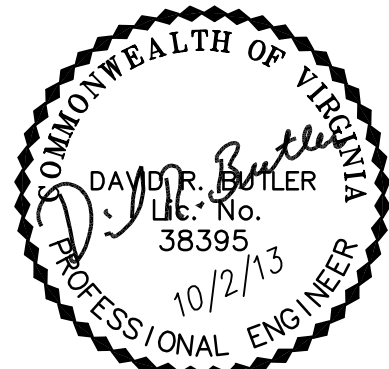
- GENERAL NOTES:
- All materials and construction methods shall conform to the Hampton Roads Planning District Commission (HRPDC) Regional Standards, fifth edition, as amended by the City of Portsmouth Special Provisions and any other applicable City Ordinance or Code.
 - The Contractor is responsible for locating all public or private utilities, which lie in the construction area prior to any excavation or construction. Any changes to the proposed Utility alignments shall be approved by the Engineer. The Contractor shall be responsible for the repair, at his expense, of all existing utilities damaged during construction.
 - The Contractor shall use only approved material in the backfill of utility trenches.
 - All utility trenches shall be backfilled and compacted to within .33' of final subgrade elevation and graded to drain. Excess material shall be removed at the Contractor's expense. All finished slopes in utility easements or in right-of-way not subject to paving shall be topsoiled and seeded in accordance with the current HRPDC and City of Portsmouth specifications and shall not exceed the maximum as follows - cut slope 4:1, fill slope 4:1.
 - The Contractor shall provide temporary drainage to relieve areas that may cause damage to the roadways, and erosion protection during construction as directed by the City of Portsmouth, the HRPDC Regional Standards, and Virginia Erosion and Sediment Control Handbook.
 - All concrete shall be class "A3" air entrained (3,000 psi) unless noted otherwise.
 - All storm sewer pipe shall be as specified on the plan sheets and shall conform to current HRPDC and City of Portsmouth Standards. All pipes shall be reinforced concrete tongue and groove.
 - Prior to construction or excavation, the contractor shall call "Miss Utility" at 1-800-552-7001. In addition, the contractor shall call the offices of any and all public or private utilities and request location of utilities that may exist and cross through the construction area, whether or not said utilities are shown on these plans. Utility companies shall be notified 48 hours in advance of any excavation in the proximity of their utilities. The contractor is responsible for the repair, at his expense, for any damage caused to utilities during construction.
 - All storm sewer pipes, drop inlets and catch basins shall be cleaned of debris and eroding material during the last stage of construction.
 - Gutterbuddy, or approved equal, inlet filter shall be placed around all existing and proposed drainage inlets.
 - Any defective, faulty, cracked, or broken walks, driveways, handicapped ramps or curb and gutter, as determined by the Engineer, shall be removed and replaced to the nearest joint prior to final acceptance at no additional expense to the City. Patching is not acceptable.

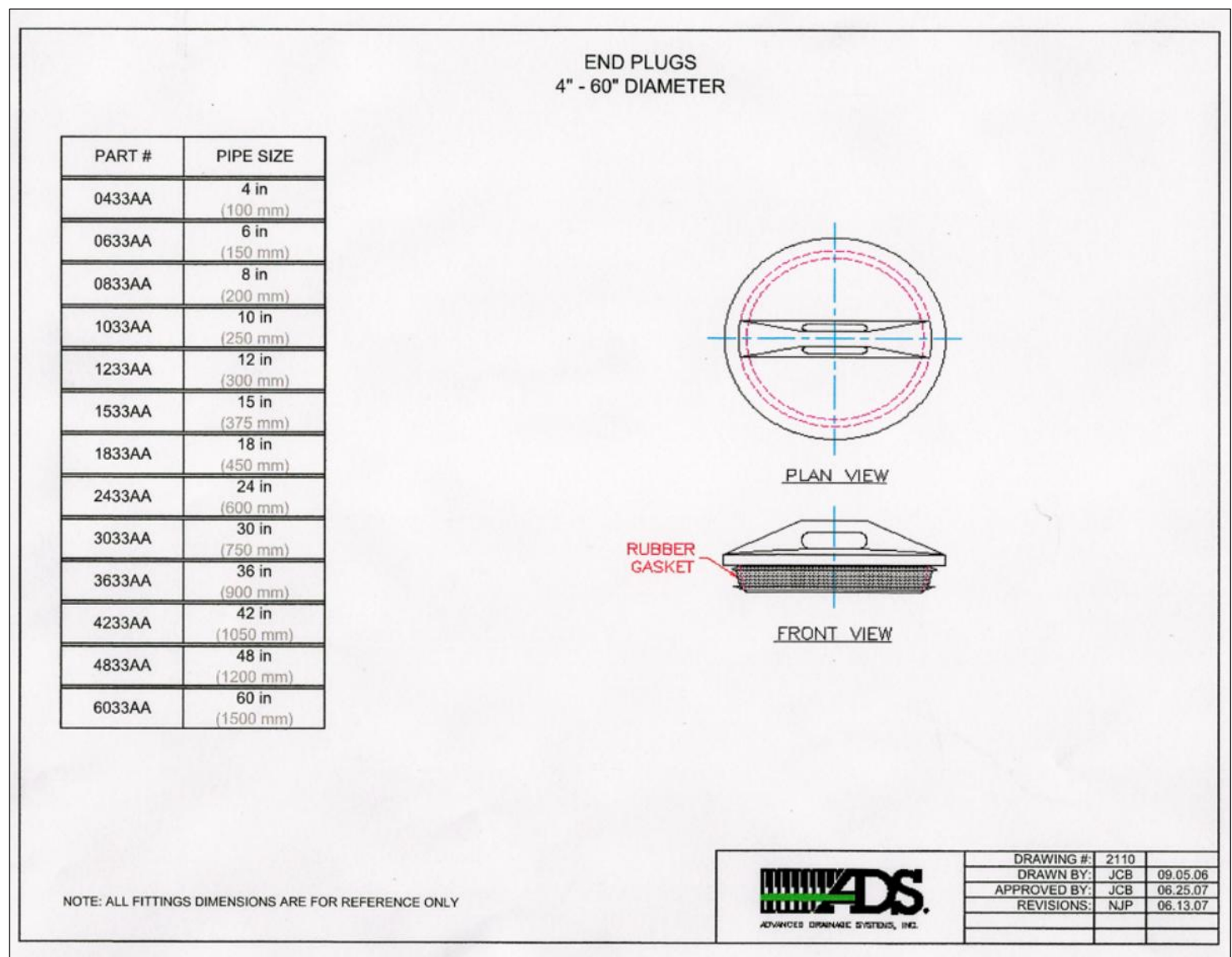
- Any items or instructions, which are noted on the plans but are not included in the Bid Price Schedule shall not be paid for separately, but shall be included in other bid items. Frames and covers for sewer manholes and drainage structures shall be by Capital Foundry, Dewey Brothers, or approved equal.
- All curb and walks to be removed shall be taken out to the nearest joint. All new walk limits shall be determined in the field and approved by the Engineer.
- Relocation, removal and/or replacement of all signs shall be coordinated with the Department of Traffic Engineering.
- All conflicting private utilities, lines and poles will be relocated by others.
- Contractor shall remove and reset all mailboxes as required (non pay item).
- All concrete drives shall be 7" thick minimum from roadway to the right-of-way. Concrete drives extending past the right-of-way shall be 4" thick minimum (See Plans for locations).
- Contractor is responsible for coordinating closure of driveways with individual property owners and must provide access to the houses.
- Contractor shall protect all trees and shrubs as directed by the Engineer.
- Removal of existing utilities in same trench as proposed utilities shall not be a pay item.
- All utility and storm drain lines must be inspected by the Engineering Department prior to backfilling.
- Disposal of excess material within the City of Portsmouth shall require prior approval from the Engineer. Prior to construction within any existing public right-of-way the contractor shall obtain a permit from the Engineering Department, City of Portsmouth, Virginia. A copy of the approved traffic control plan is to be submitted with the right-of-way permit application.
- The contractor shall be responsible for replacing with matching materials any pavement, driveways, walks, curbs, etc., that must be cut or that are damaged during construction.
- When materials which are unsuitable for foundations, subgrades, or other roadway purposes occur within the limits of street construction, the contractor shall be required to excavate such materials below the grade shown on plans and the areas so excavated shall be back filled with approved suitable materials. The extent of undercutting and backfilling to be determined by the Engineering division, City of Portsmouth, Virginia.
- Replacement of pavement shall be in accordance with standard pavement patching details (STD. Drawing 7.1 or 7.2) Specifications and standards for the Department of Public Works, or in accordance with the right-of-way permit specifications, Engineering Department, City of Portsmouth, Virginia.
- The contractor shall become completely familiar with the project conditions and proposed work. The information provided on these drawings is for use by the City and the Inspector and is provided by the City to the contractor for informational purposes. The information contained within the Contract Documents and on these drawings shall be used by the contract at their own risk.

- SPECIAL NOTES
- Maximum allowable slopes on driveways shall be 12:1. Driveways shall be placed to nearest joint. Contractor to verify limits of all drives with the Engineer.
 - Preserve all power poles not in conflict. Coordinate relocation of conflicting power poles with the Engineer and company. Cost of utility pole relocations shall be by utility owner.
 - All drives shall be concrete in the R.O.W.
 - There shall be a minimum of six inches between adjacent driveway entrance aprons as measured at the curb.
 - Removal and replacement of gravel drives and tie-ins at the edge of aprons is the responsibility of the contractor. Coordinate limits of work with the Engineer. Drives shall be a minimum of 4" gravel beyond existing R.O.W. (see plans for locations).
 - All water meters and sanitary sewer cleanouts must be set behind the curb within the City right-of-way.
 - Coordinate replacement of outdated meters with the Engineer and the City Public Utilities Department.
 - All fence removal and replacement shall be coordinated by the Engineer and homeowner.
 - The Contractor shall adjust the tie-in length for new walks to accommodate steps as directed by the Engineer.
 - The Contractor shall remove and replace curb and gutter as necessary to complete utility work. Curb and gutter shall be replaced in 10 foot sections. The cost of replacing this curb and gutter will not be measured separate for payment and will be included in the respective utility pay item.
 - All items of work required by the documents to complete the project, but not specifically included in a pay item shall be considered an incidental item in accordance with Specification Section 109.

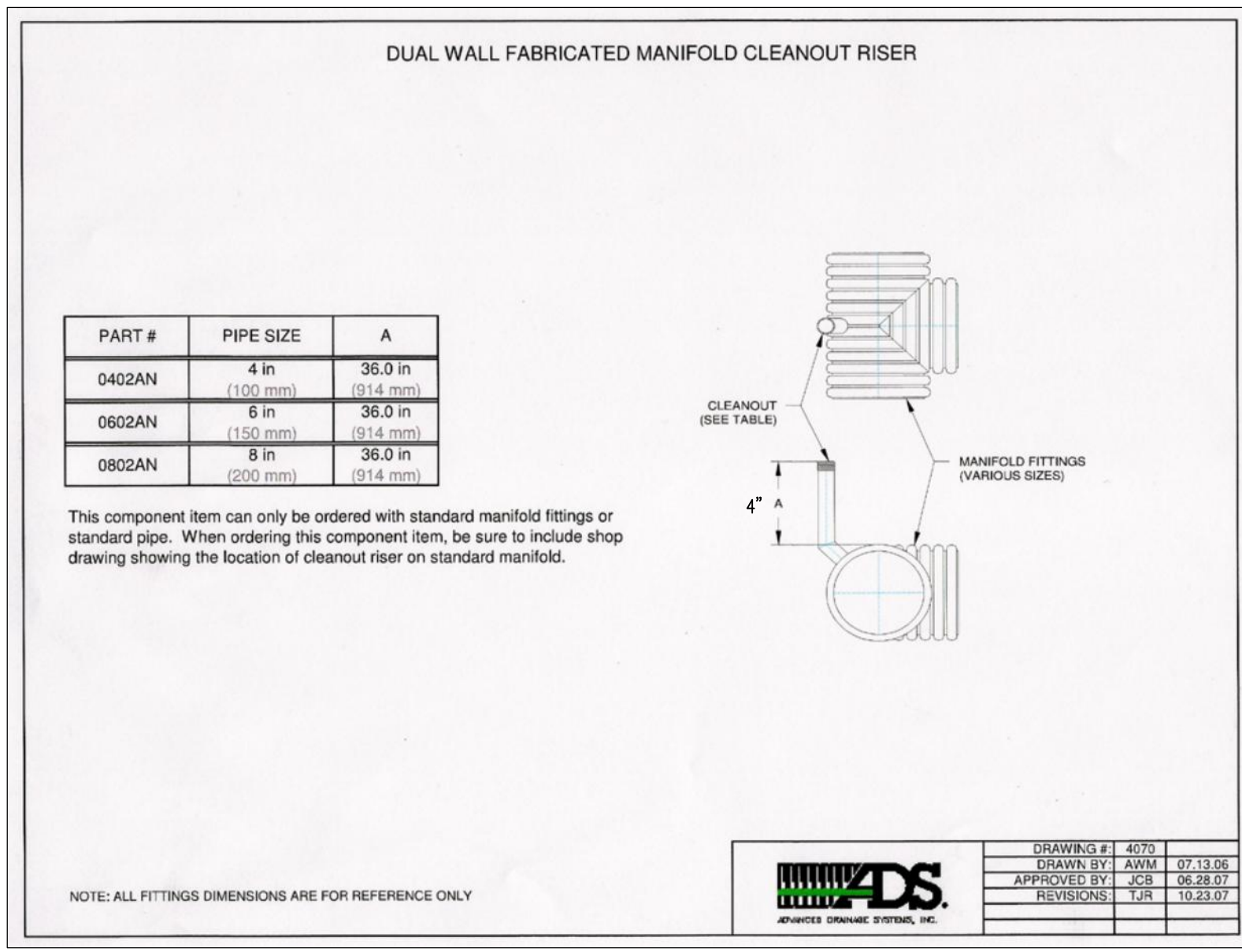
UTILITY DETAILS AND NOTES PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: N/A	SHEET 8 / 13
DATE	COMMENT	FILE NO.:	C8
REVISION SCHEDULE			

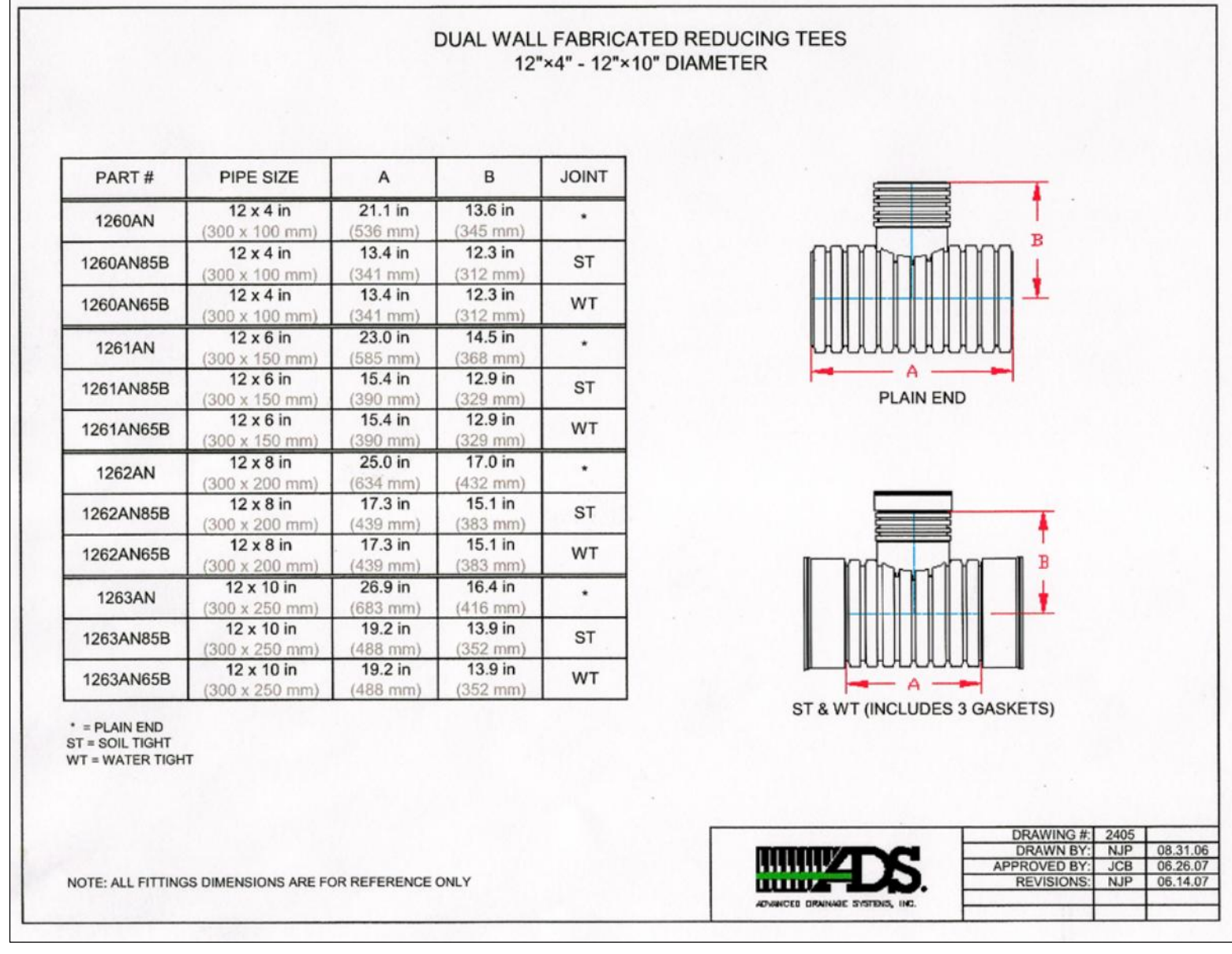




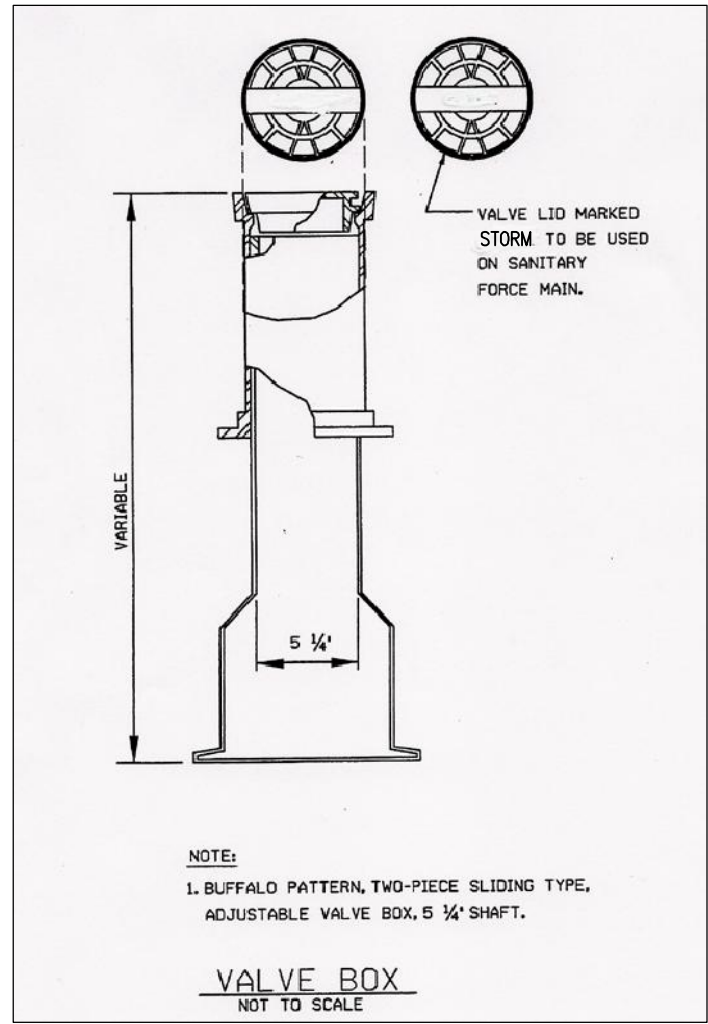
THIS DETAIL TO BE USED FOR THE 6" & 12" PLUGS FOR OBSERVATION WELL CAPS



THIS DETAIL TO BE USED FOR THE OBSERVATION WELLS



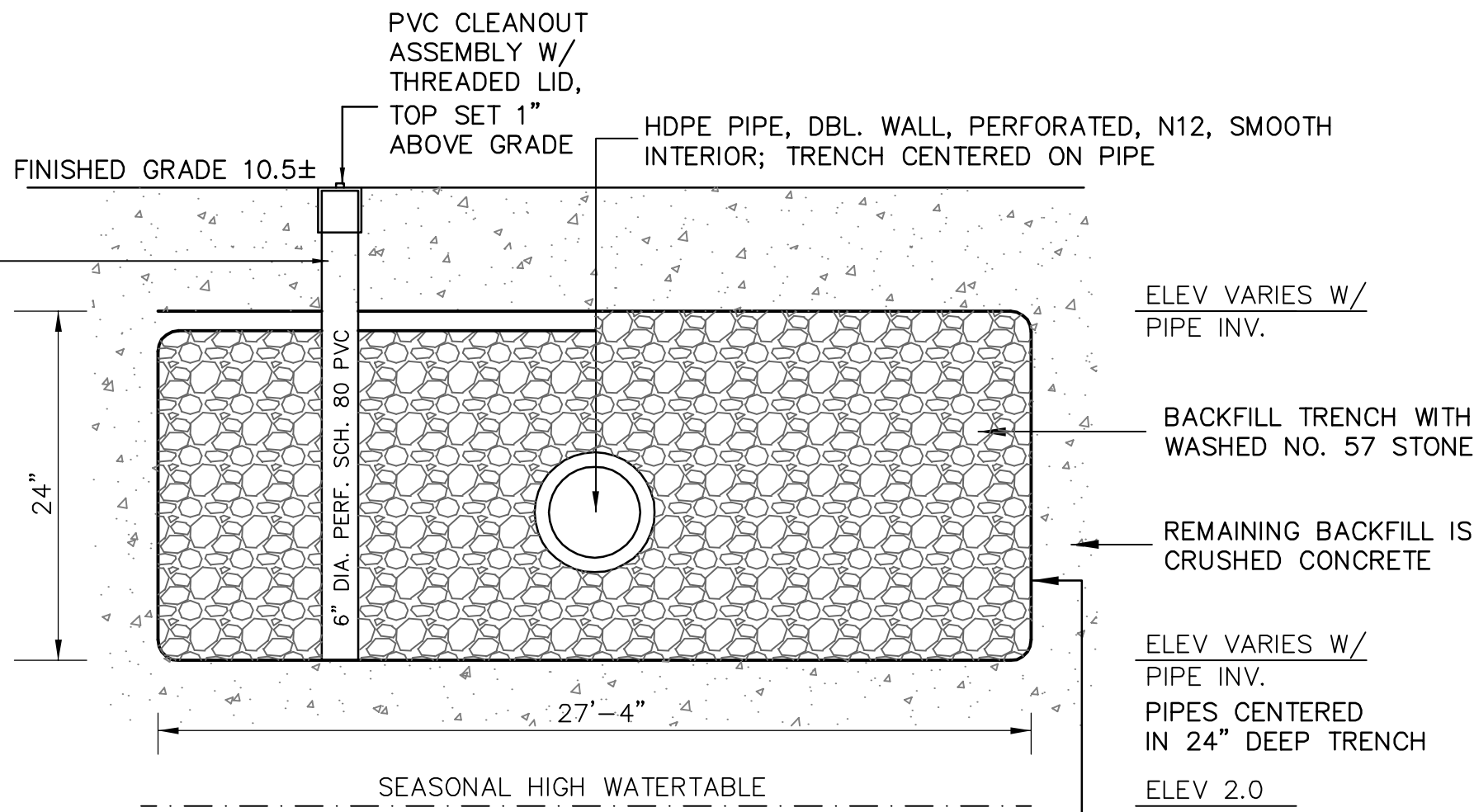
THIS DETAIL TO BE USED FOR THE 6" X 12" TEES



BMP MAINTENANCE SCHEDULE

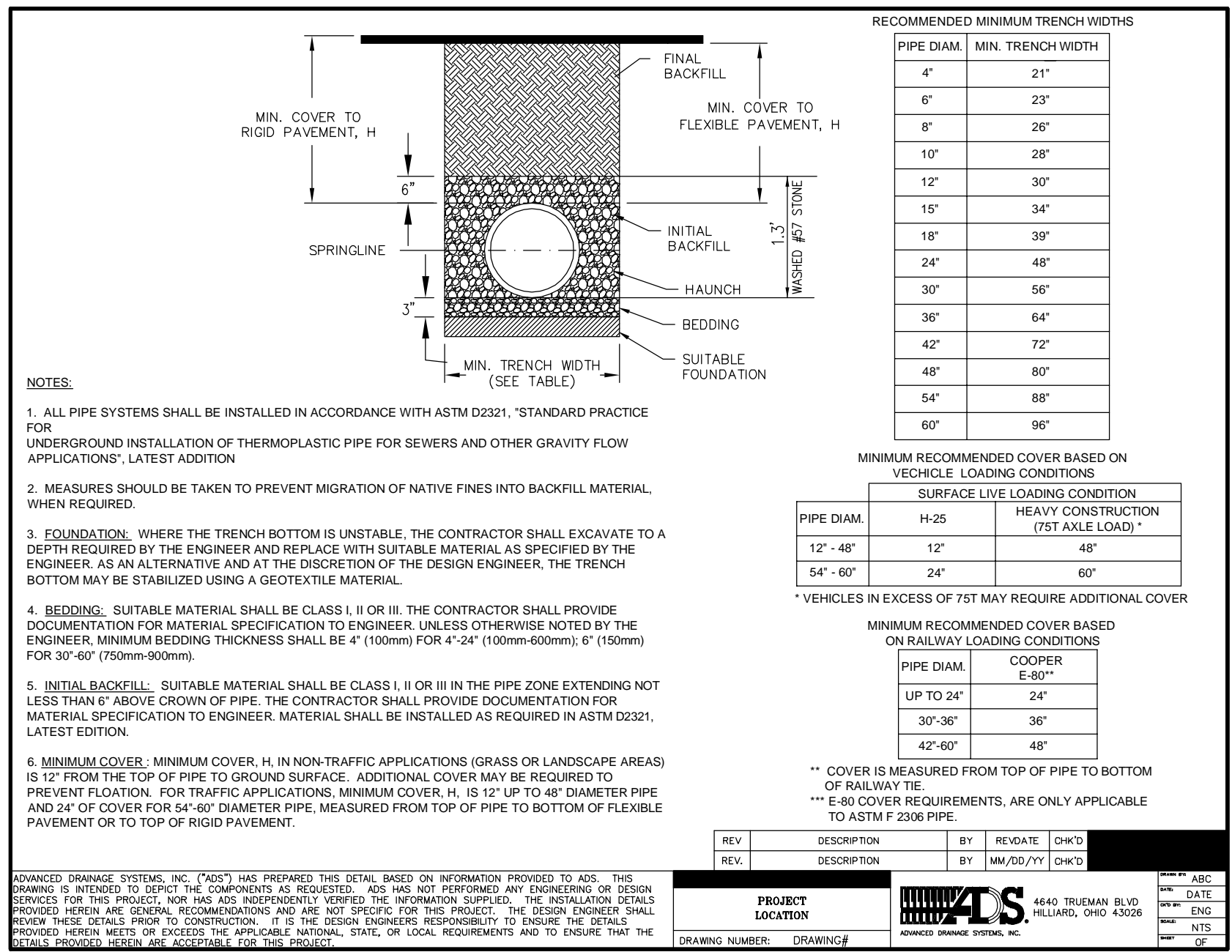
1. INSPECT BMP INFILTRATION SYSTEM MONTHLY AND AFTER MAJOR STORM EVENTS FOR DEBRIS.
2. OBSERVATIONS WELLS SHOULD BE CHECKED EVERY 3 MONTHS FOR CONTAMINATION, WITH MAINTENANCE SCHEDULED AT MINIMUM SIX-MONTH INTERVALS.
3. SHOULD TRENCH FAIL TO DRAIN IN A REASONABLE AMOUNT OF TIME, (48-72 HOURS) OWNER SHALL HAVE PERFORATED PIPES JETTED AND VACUUMED VIA 4" OBSERVATION WELLS AND INLETS.
4. IN THE EVENT OF COMPLETE FAILURE OF THE BMP INFILTRATION FACILITY, I.E., WATER FAILS TO EXFILTRATE WITHIN 72 HOURS AND IS VISIBLE FROM THE OBSERVATION WELLS, THE FILTER FABRIC AND DRAIN SOCKS SHALL BE EXCAVATED, AND REPLACED UTILIZING THE ORIGINAL DESIGN INVERTS AND DIMENSIONS.
5. THE OWNER SHALL KEEP A LOG OF THESE INSPECTIONS ON LOCATION FOR REVIEW BY THE CITY OF PORTSMOUTH, DEPARTMENT OF PUBLIC WORKS.
6. THE TOP 6" OF SURFACE SURROUNDING EACH STORM INLET SHOULD CONSIST OF 57 STONE ONLY, NO CRUSHED CONCRETE, IN ORDER TO PREVENT FINES FROM ENTERING THE INLETS AND CAUSING FAILURE. MINIMUM AREA OF 57 STONE AROUND EACH INLET SHOULD BE 30' DIAMETER OR GREATER.

6" DIAMETER PERFORATED SCH. 80 PVC; PERFORATIONS TO BE 3/8" DIA., SPACED ON STAGGERED ROWS 4" C-C. PROVIDE "DRAIN SOCK" OR EQUAL ON ENTIRE PERFORATED PIPE TO EXTEND FROM FINISHED GRADE SURFACE TO THE BOTTOM OF THE INFILTRATION TRENCH



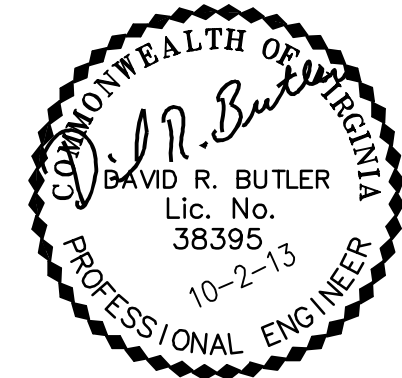
SEE SHEET 2 FOR PIPE INVERTS, LENGTHS, SLOPES, ETC.

DETAIL INFILTRATION BEST MANAGEMENT PRACTICE WITH OBSERVATION WELLS NO SCALE



ADS PERFORATED N12 HDPE PIPE BEDDING DETAIL (EXCLUSIVE OF STRUCTURES 12-22)

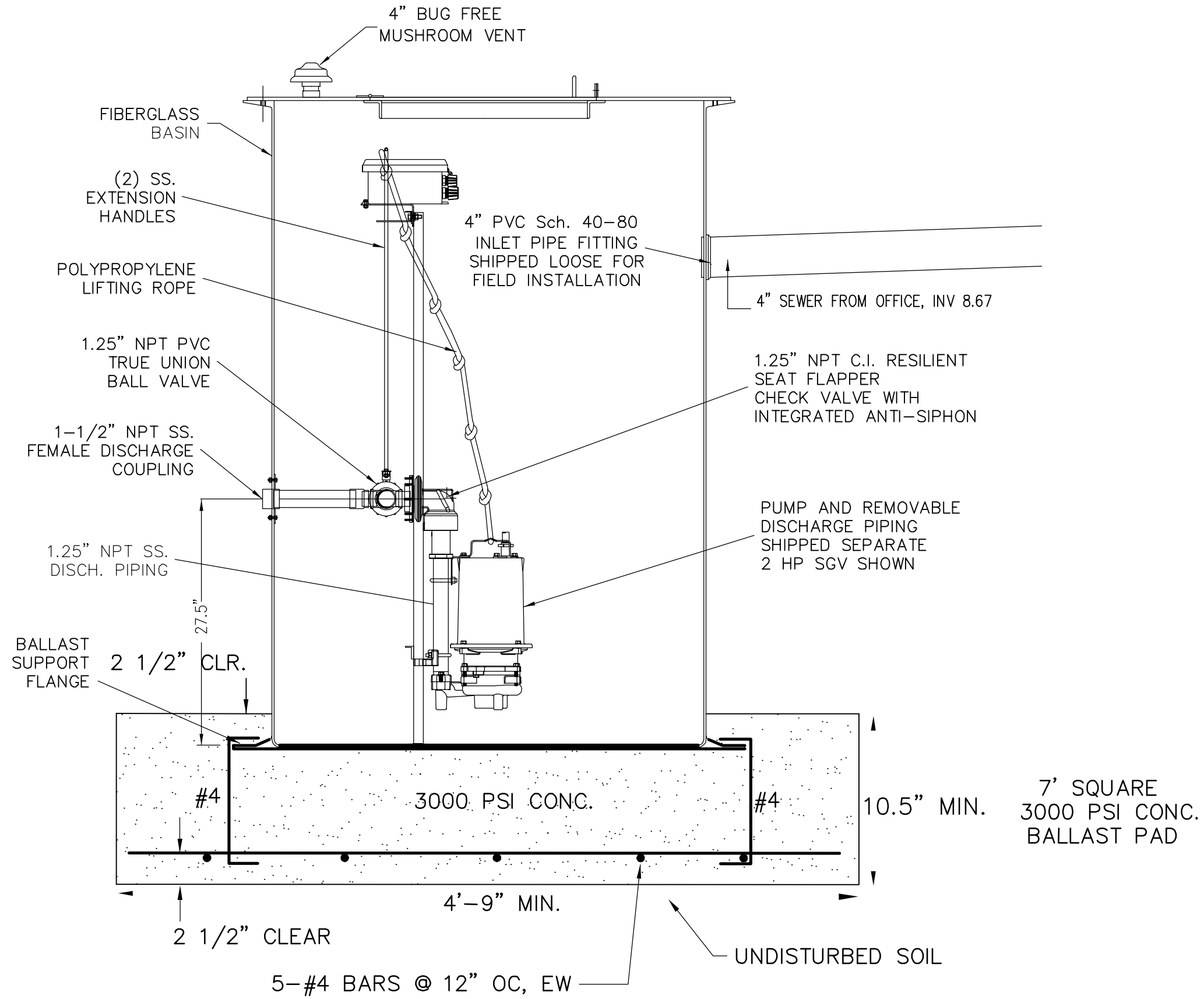
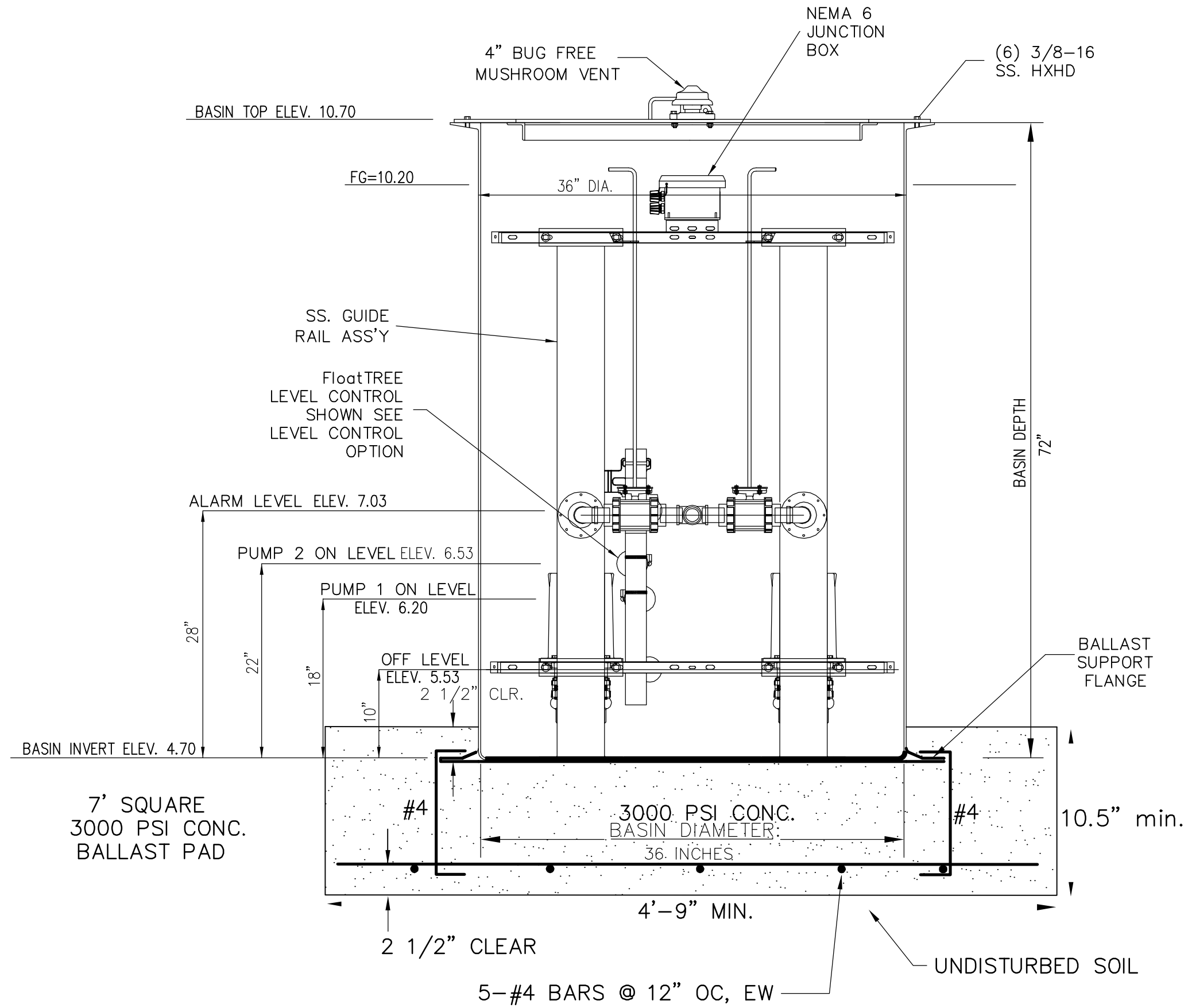
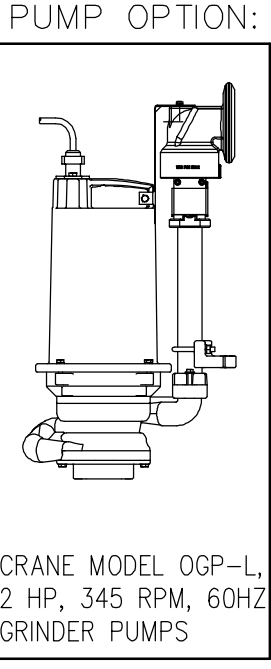
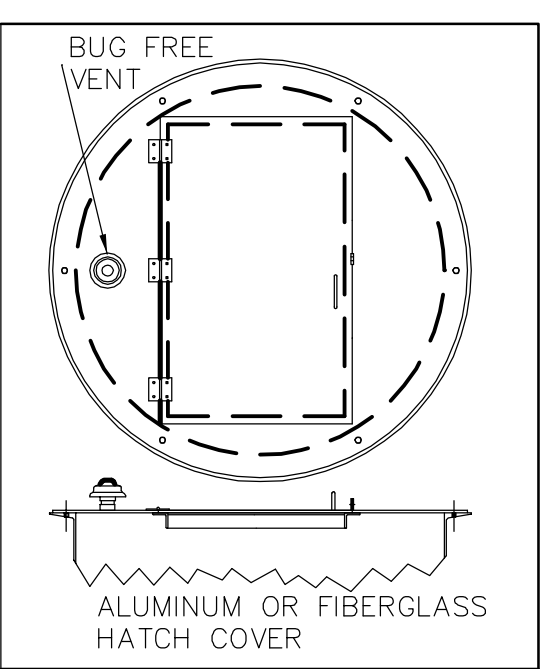
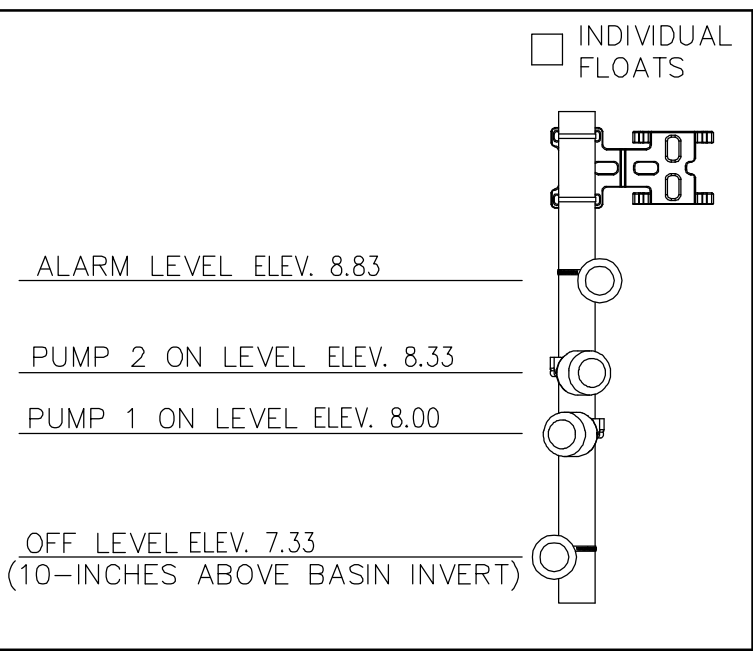
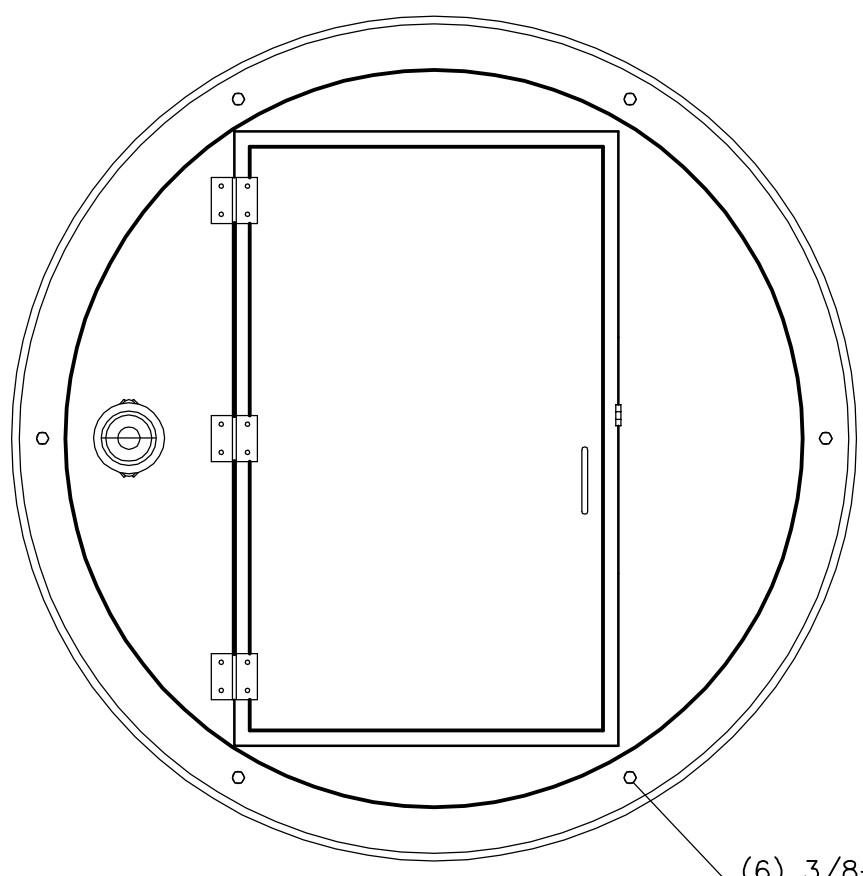
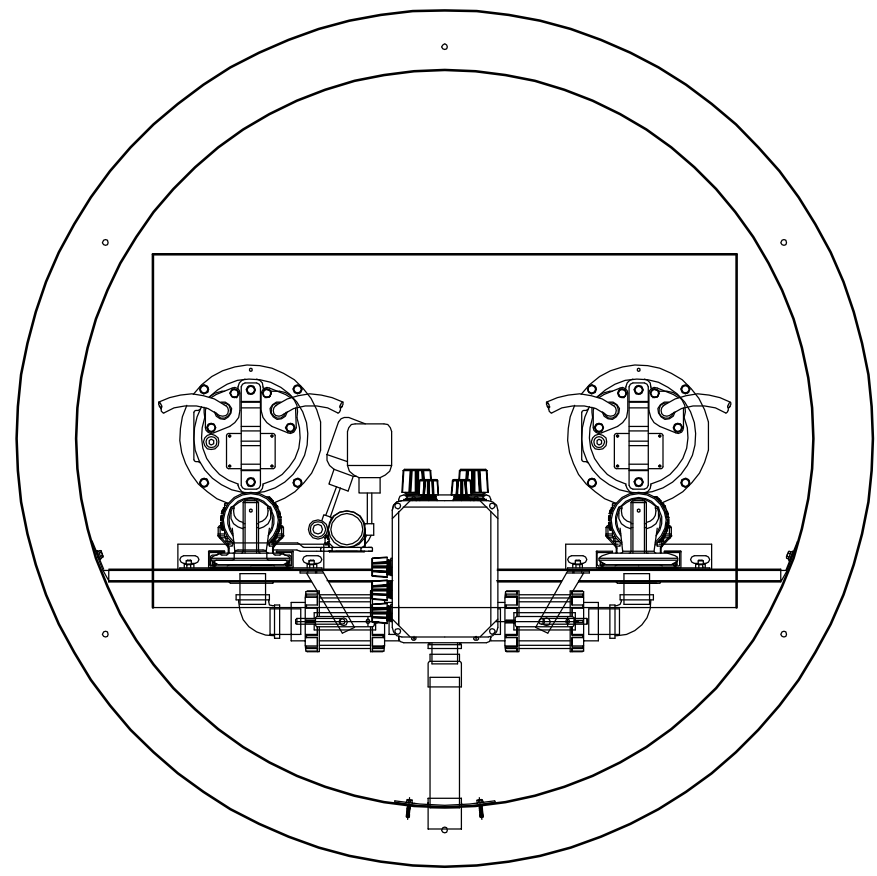
HDPE PIPE SHALL BE DUEL WALL, SMOOTH INTERIOR, N-12
BY ADVANCED DRAINAGE SYSTEMS, INC., OR APPROVED EQUAL



BMP NOTES & DETAILS

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE: OCTOBER 2, 2013
9/19/12 REVISE PROJECT NAME		7/12/12 DSC REVIEW	
4/25/12 DSC REVIEW		DATE COMMENT	
REVISION SCHEDULE		GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX	
SCALE: 1" = 10'		FILE NO.:	SHEET 9/13
		C9	

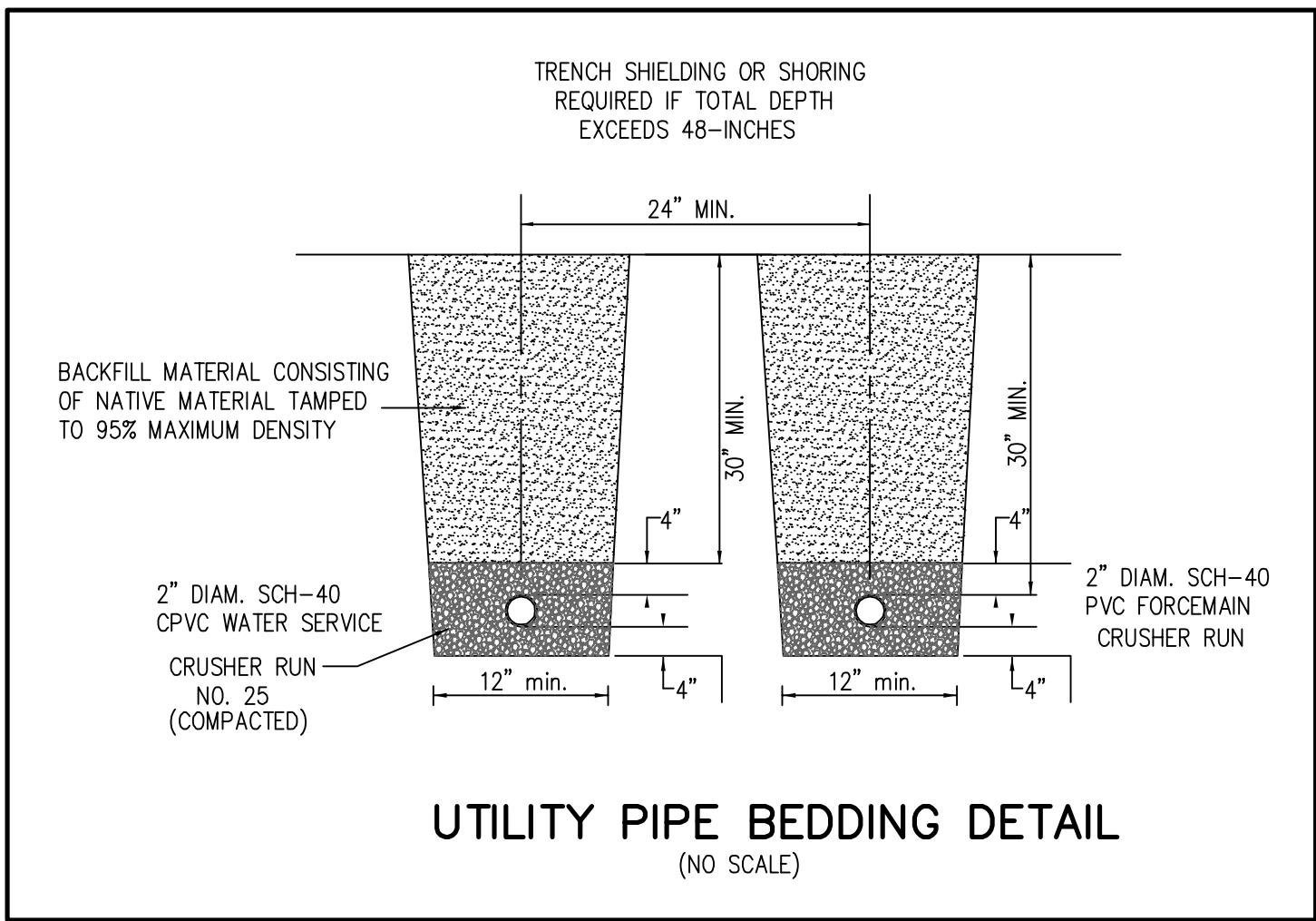


Pump Station Notes:

- Furnish and install a submersible duplex grinder pump station in accordance with the specifications. The pump shall be equipped with a 2 HP submersible electric motor. The pump shall be capable of delivering 30 GPM at 31 feet of head. Pump shall be a Crane Series OGP-L, 2 HP Grinder Pump, Single Phase, 240 V, or equal. Low voltage protection shall be provided for the motor. Installer to verify available power before ordering pumps. Impeller size: 4-inch.
- Exfiltration: All force mains shall be tested at a minimum pressure of at least 50% above the design operation pressure. Leakage shall not exceed the amount driven by the following formula: $L = ND \sqrt{1/2} \sqrt{3700}$ Where L is allowable Leakage in gallons per hour N is the number of pipe joints D is the Pipe Diameter in inches P is the Test Pressure in PSI. The contractor shall test the pump station and force main for a minimum of 30 minutes.
- Audio and visual alarm system must be provided with and alarm test function. The alarm shall be on an independent circuit. The alarm system at the station shall be equipped with an alarm test function. Alarm shall monitor high water and power failure.
- NEMA 1 control panel to be located on the exterior wall and mounted in accordance with the NEC.
- Electrical service outlet receptacle shall be available in the vicinity of the pump station.
- A backflow prevention device will be provided on any faucet within 50 feet of the pump station.
- Provide minimum of 185 gal. of storage between alarm level and overflow elevation (top of station) within the pump well.
- A back-up power supply for the alarm system shall be provided with a minimum capacity of 24 hours.
- A weatherproof sign, containing notification procedures in the event of pump failure, shall be placed adjacent to the audio / visual alarm.

NOTES :

- ALL DIMENSIONS TO BE $\pm 1/4"$ UNLESS OTHERWISE SPECIFIED.
- CONTACT STUART TAYLOR, TENCARVA MACHINERY CO. TO COORDINATE SALES AND DELIVERY OF EQUIPMENT
933 CORPORATION LANE
CHESAPEAKE, VA. 23320
757-548-0400
EMAIL: STAYLOR@TENCARVA.COM



PACKAGE PUMP STATION DETAILS

THIS PRINT IS AND CONTAINS PROPRIETARY INFORMATION OWNED EXCLUSIVELY BY CRANE PUMPS & SYSTEMS, INC. THIS RESTRICTION INCLUDES, BUT IS NOT LIMITED TO THE CONDITION THAT THIS PRINT WILL ONLY BE USED AS A RECORD OR TO IDENTIFY OR INSPECT PARTS OR FOR OTHER INFORMATION PURPOSES, AND WILL NOT BE USED TO MANUFACTURE OR PROCURE THE MANUFACTURE OF THE PARTS SHOWN IN THIS PRINT BY ANY OTHER SOURCE THAN CRANE PUMPS & SYSTEMS, INC.

AS A RESULT OF BARNES CONSTANT PRODUCT IMPROVEMENT PROGRAM, PRODUCT CHANGES MAY OCCUR. AS SUCH, BARNES RESERVES THE RIGHT TO CHANGE PRODUCT WITHOUT PRIOR WRITTEN NOTIFICATION

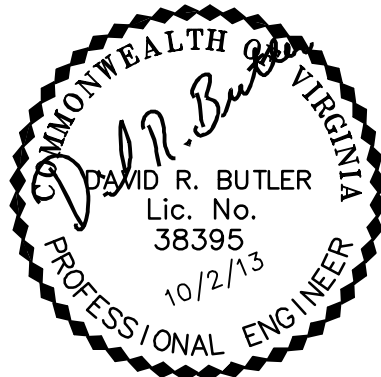
WWW.BARNESPUMPS.COM

REV
A

CRANE®

PUMPS & SYSTEMS

BARNES®
PRESSURE
SYSTEMS



DATE	COMMENT
REVISION SCHEDULE	

PUMP STATION DETAILS

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: NO SCALE	SHEET 10/13
FILE NO.:		C10	

"C" Channel Guide Rails for For 1½" NPT Moveable Fittings

www.cranepumps.com

15-001

Accessories

"C" Channel Guide Rails for 1½" NPT Discharge Simplex or Duplex

Specifications:

The "C" channel guide rail assembly is made of 300 series stainless steel. The guide rail mounts to the upper and lower horizontal brackets attached to the basin wall. The rail also rest on the bottom of the basin floor. The stainless steel guide rail supports the pump's required discharge from the basin floor. Guide brackets (installed with the Moveable Fitting Assembly) are attached to the pump for positioning of the unit on the guide rail during installation and removal.

The stationary of the hydraulically sealed discharge is powder coated machined cast iron. The stationary fitting has a fiber reinforced neoprene diaphragm clamped between the stainless steel rail and the stationary pressure vessel. The moveable fitting is held against the stationary fitting by the construction of the stainless steel rail, aligning the moveable fitting to the flexible diaphragm for proper sealing of the two surfaces.

Each assembly includes:

- 300 Series Stainless Steel Guide Rail
- 300 Series Stainless Steel Upper and Lower Support Brackets
- Available For Basin Depths 4" to 16" (1.2M to 3.9m)
- 300 Series Stainless Steel Intermediate support Brackets for Basin Depths 14" (3.7m) and Greater
- Powder Coated Cast Iron Stationary Fitting
- Fiber Reinforced Neoprene Diaphragm

Quantity of One (1) each for Simplex and Two (2) for Duplex.

SECTION #
PAGE
DATE 11/03

CRANE PUMPS & SUPPLY

www.craneumps.com

PS-051

Specifications:

DISCHARGE	1½" NPT, Vertical, Ball-Joint Flange
LIQUID TEMPERATURE	104°F (40°C) Continuous
VOLUME	Cast Iron ASTM A-48, Class 30
MOTOR HOUSING	Cast Iron ASTM A-48, Class 30
SEAL PLATE	Cast Iron ASTM A-48, Class 30
IMPELLERS:	
Design:	12 Vane, Vortex, With Pumps Out Vokes On Back Side, Dynamically Balanced, ISO C63
Material:	56-5-5 Bronze
IMPELLER SPACER	300 Series Stainless Steel
SHREDDING RING	Hardened 40C Stainless Steel
CUTTER	Hardwelded C-65, Hardened 40C Stainless Steel, Rockwell C-65
SHAFT	416 Stainless Steel
SQUARE RINGS	Rockwell N
HARDWARE	300 Series Stainless Steel
PAINT	Oil Free Dryness
SEAL:	
Design:	Sing's Mechanical
Material:	Rotating Faces - Silicon Carbide Stationary Faces - Silicon Carbide Bashmore - Bash-N Hardwelds - 300 Series Stainless 20-1 (B) Im-Jet, Corst. Custom Molded Quick Connect, for Sealing and Strain Relief
CORD ENTRY	Manual: CSA/UL Approved 1232 Type 50W
CORD	
UPPER BEARING:	Design: Single Row, Angular contact Ball Lubrication: Oil Load: Radial & Thrust
LOWER BEARING:	Design: Single Row, Angular contact Ball Lubrication: Oil Load: Radial & Thrust
MOTOR:	Design: NEMA-1-Single Phase Torque Curve, Off-Flide, Squirrel Cage Induction Fan Insulation: Capacitor Start/Capacitor Run.
SINGLE PHASE	

Model OGPR
Reduced Vortex

Submersible Grinder Pumps

Series: OGP
7HP, 3450RPM, 60Hz


CSA 100-File No. LR16667
UL 718

DESCRIPTION:

THE GRINDER PUMP IS DESIGNED TO
REDUCE DOMESTIC SEWAGE TO A FINELY
GROUND SLURRY.

CRANE PUMPS & SYSTEMS

SECTION A
DATE 3/07

SECTION 1
RESURFACING SYSTEMS

 www.craneumps.com

Fiberglass Ballast Support Flange
 With Ballast Support Flange

Accessories

PG-015

Specifications:

Basin construction is custom molded fiberglass reinforced polyester resin.

The wall thickness shall be sufficient to withstand a water-saturated sand load of 120 lbs per cubic foot (1.9 graticu. cm) with a 1.5 safety factor.

The Ballast support flange shall extend a minimum of three inches (76mm) to the outside of the basin. The flange is designed to the bottom of the basin. When secured properly to a concrete pad or pouring concrete over and around the flange, prevents the basin from rising, or floating out of the ground when empty as a result of static ground pressure.

The basin will withstand a maximum temperature of 150°F (66°C).

CRANE
 A Crane Co. Company

PUMPS & SYSTEMS

USA: (877) 778-8947 • Canada: (905) 457-8223 • International: (937) 615-3598

SECTION #
PAGE 1
DATE 1/03

True Union Ball Valves

1½" NPT

Division 2000
PRESSURE TRANSDUCERS

www.craneumps.com

Accessories

PS-08

An isometric line drawing of a True Union Ball Valve. It features a large, T-shaped handle with a knurled grip, attached to a cylindrical valve body with a flange at the bottom.

True Union Valves

1½" NPT

P/N: 085115

A line drawing of an L-shaped extension handle. It has a long, straight vertical stem and a shorter horizontal grip at the top.

Extension Handles

A logo for ISO 9001 Registered Supplier. It features the text "ISO 9001" above "Registered Supplier" and "MEMBER" below it, all enclosed in a rectangular border.

Specifications:

True Union Ball Valves:

The True Union Ball Valves are manufactured of Type I Schedule 80 PVC. (Ball Classification 12554-B) with EPDM Gaskets for superior chemical and corrosion resistance. These valves are rated at 150 PSI, (10.6 kg/cm²) non-druck, with a maximum operating pressure at 73°F (23°C). The valves are of quick disconnected design for maintenance and can be reporable to the component level, also full port bore, 1/4 turn, leak tight shut-off and are listed by NSF for use in potable water service.

Extension Handle:

Made From 3/8" (10mm) diameter 304 series stainless steel and can be used with 1½" NPT true union ball valves.

SECTION F
PAGE 14
DATE 11/03

CRANE

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PUMPS & SYSTEMS

USA: (937) 778-8947 • Canada: (905) 457-6223 • International: (937) 615-3598

Level Controls

Individual Floats Assembly,™ Duplex for Barnes™ C™ Channel Rail System

Accessories

Individual Floats Assembly

The universal mounting bracket allows the individual floats to be located on either side of the C™ channel rail for ease of installation around existing inlets or other obstructions.

Specifications:

The Mercury Level Controls are pilot duty devices which control the function of motor load devices, such as contactors, motor starter and power relays, to automatically cycle a pump or pumps. They can also be used for alarm signaling devices.

Gly.: 4 floats for Pump, Pump Off, Pump 1 On, Pump 2 On, Alarm

Floats Assembly:

CORD 192 SJOW, 29 (7.4mm) Dia

Mounting Clip, ABS/Nylon and 300 series Banding

Float Housing Polypropylene

Temperature Rating 60° C

Float Switch Mercury, Narrow Angle, Horizontal

Float Switch Rating 4.5A @ 115VAC RES

..... 2.5A @ 220VAC RES

Pole PWC

DUPLEX WIRING DIAGRAM
OPTIONAL EQUIPMENT

SECTION #
PAGE 26
DATE 11/93

CRANE PUMPS & SYSTEMS

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USA: (637) 778-8947 • Canada: (905) 461-6223 • International: (637) 615-3598

CRANE
PUMPS & SYSTEMS
www.craneumps.com

PS-020

Movable Fitting Assembly
1½" NPT
for Stainless "C" Channel Guide Rails

Accessories

Specifications:

The Movable Fitting Assembly is used with the BARNES Stainless "C" Channel Guide Rails for installation in basins.

Each movable assembly includes:

A stainless steel upper pump bracket with stainless hardware, stainless steel pipe nipples, cast iron flapper style check valve (powder coated) with resilient seat flapper, integrated anti-siphon and a cast iron powder coated lower guide bracket.

**PUMP
MODEL**
NOT

SIZE-NPT
Inch (mm)
1.25 (32)

PART No.
W/ VALVE
116596B

Pump Not Included. Movable fitting factory assembled to pump when ordered with basin package.

Movable fitting shown with 502V pump for illustration purposes only.

Movable Fitting Assembly 1½" NPT Discharge

DESCRIPTION

THE BREAK AWAY FITTING IS DESIGNED TO ALLOW THE SUBMERGIBLE PUMP TO BE INSTALLED OR REMOVED WITHOUT REQUIRING PERSONNEL TO ENTER THE WET WELL.

CRANE

PUMPS & SYSTEMS

A Crane Co. Company

USA: (801) 378-8947 • Canada: (905) 457-6223 • International: (871) 616-5098

SECTION F
PAGE 7
DATE 11/03

DAVID R. BUTLER
Lic. No. 38395
10/2/13
COMMONWEALTH OF VIRGINIA
PROFESSIONAL ENGINEER

- ES-1: Unless otherwise indicated, all vegetative and structural erosion and sediment control practices will be constructed & maintained according to minimum standards and specifications of the Virginia Erosion & Sediment Control Regulations (4VAC50-30).
- ES-2: All erosion and sediment control measures are to be placed prior to or as the first step in clearing.
- ES-3: A copy of the approved erosion and sediment control plan shall be maintained on the site at all times.
- ES-4: Prior to commencing land disturbing activities in areas other than indicated on these plans (including, but not limited to, off-site borrow or waste areas), the contractor shall submit a supplementary erosion control plan to the owner for review and approval by the City of Portsmouth.
- ES-5: The contractor is responsible for installation of any additional erosion control measures necessary to prevent erosion and sedimentation as determined by the City Erosion & Sediment Control Inspector.
- ES-6: All disturbed areas are to drain to approved sediment control measures at all times during land disturbing activities and during site development until final stabilization is achieved, after which, upon approval of the City's Erosion & Sediment Control Inspector, the controls may be removed. Trapped sediment and the disturbed soil areas resulting from the removal of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.
- ES-7: During dewatering operations, water shall be pumped into an approved filtering device.
- ES-8: The contractor shall inspect all erosion control measures at least every 2 weeks and immediately after each runoff-producing rain event. Any necessary repairs or cleanup to maintain the effectiveness of the erosion control devices shall be made immediately.
- ES-9: The contractor is responsible for the daily removal of sediment that has been transported onto a paved or public road surface.
- ES-10: The contractor shall be responsible for preventing surface and air movement of dust from exposed soils which may present health hazards, traffic safety problems, or harm animal or plant life.

ALL LAND DISTURBING ACTIVITIES MUST CONFORM WITH THE APPLICABLE REGULATIONS OF THE CITY OF PORTSMOUTH CODES, ORDINANCES, AND PWSS AND THE VIRGINIA DEPARTMENT OF CONSERVATION AND RECREATION EROSION AND SEDIMENT CONTROL HANDBOOK. THE CONTRACTOR SHALL EXERCISE EVERY REASONABLE PRECAUTION, INCLUDING THE APPLICATION OF TEMPORARY AND/OR PERMANENT MEASURES TO ASSURE EROSION CONTROL DURING AND AFTER CONSTRUCTION TO CONTROL EROSION AND PREVENT/MINIMIZE SEDIMENT RUNOFF. THE ENGINEERING DEPARTMENT/PERMITS AND INSPECTIONS DIVISION SHALL ENFORCE THESE REQUIREMENTS. THE CITY INSPECTOR RESERVES THE RIGHT TO REQUIRE OTHER MEASURES NOT SPECIFICALLY DESCRIBED HEREIN TO CORRECT ANY EROSION OR SILTATION CONDITION.

Fabric Properties ¹	Light-Duty Entrance ² (Graded Subgrade)	Heavy-Duty Entrance ² (Rough Graded)	Test Method
Grab Tensile Strength (lbs.)	200	220	ASTM D1682
Elongation at Failure (%)	50	220	ASTM D1682
Mullen Burst Strength (lbs.)	190	430	ASTM D3786
Puncture Strength (lbs.)	40	125	ASTM D751 (modified)
Equivalent Opening Size (mm)	40-80	40-80	U.S. Standard Sieve CW-02215

³ **Heavy Duty Entrance:** Sites with only rough grading and where most travel would be multi-axle vehicles. Examples of fabrics which can be used are: Trevira Spunbond 1135, Mirafi 600X, or equivalent.

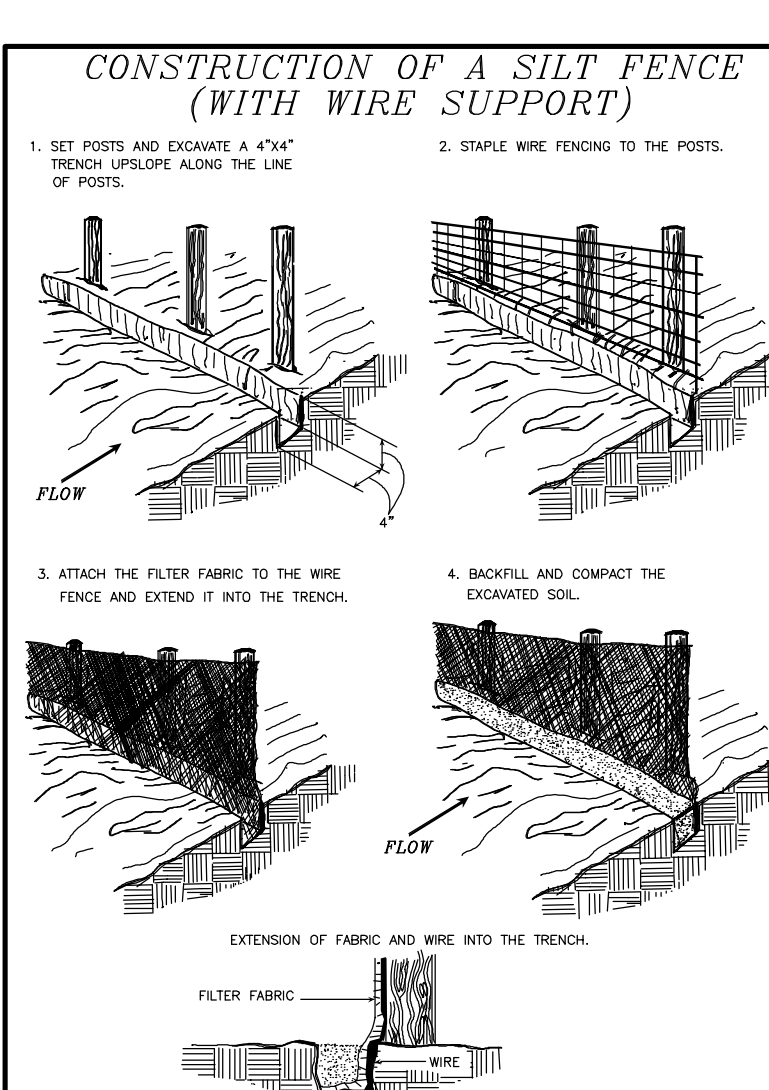
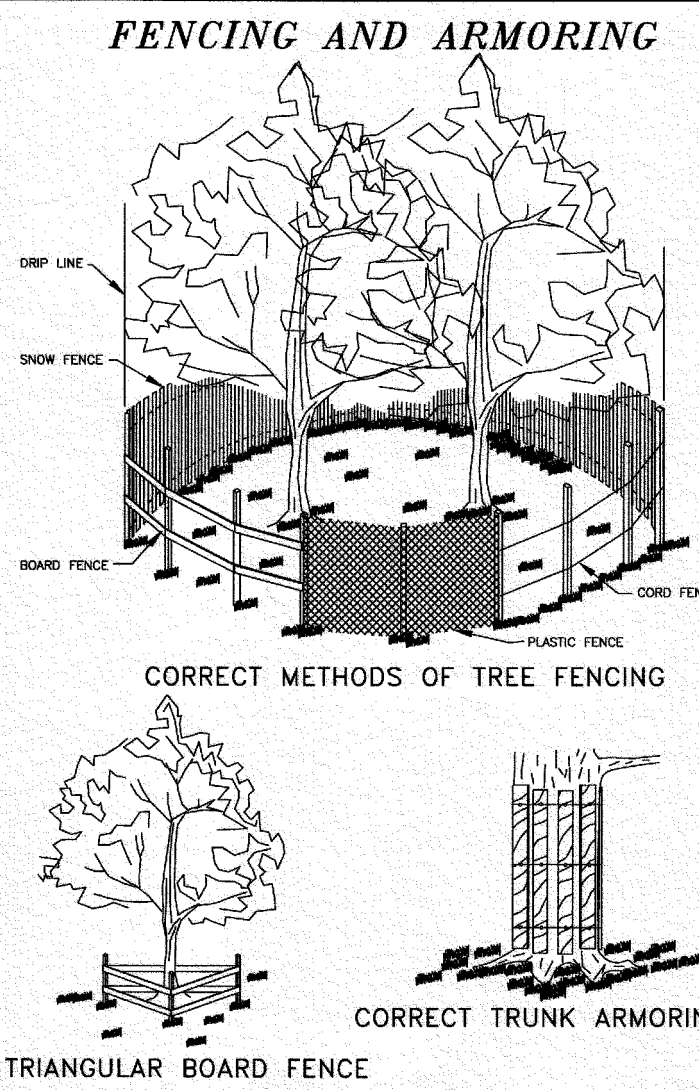
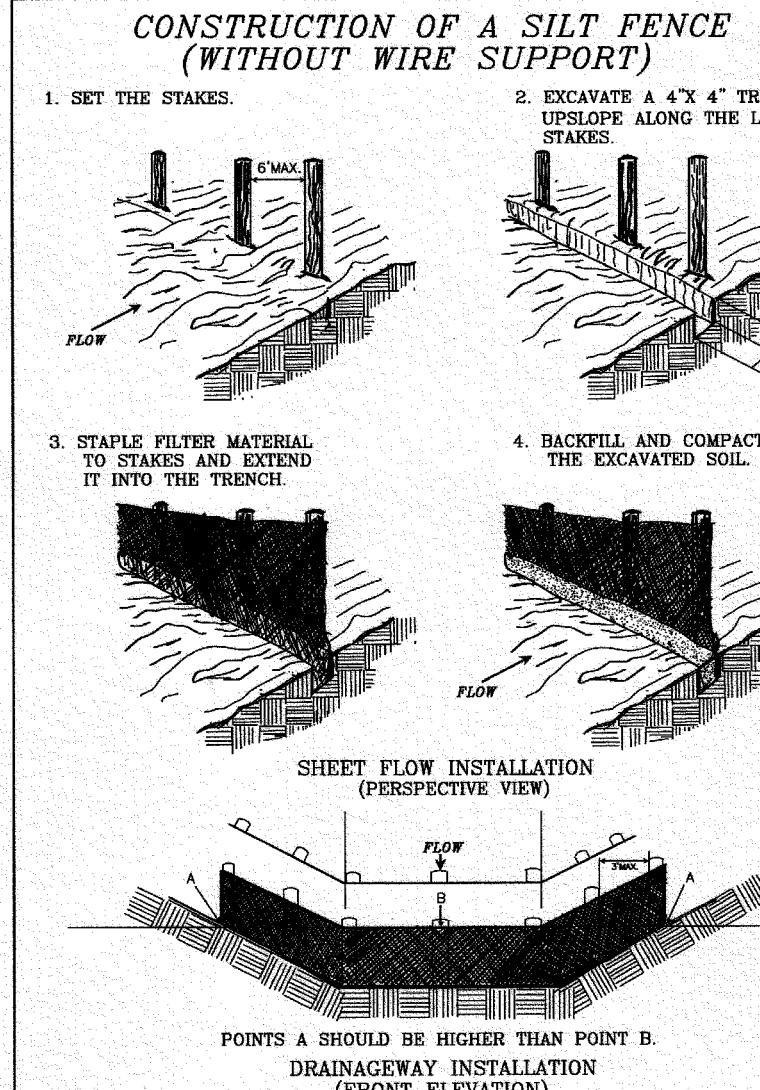
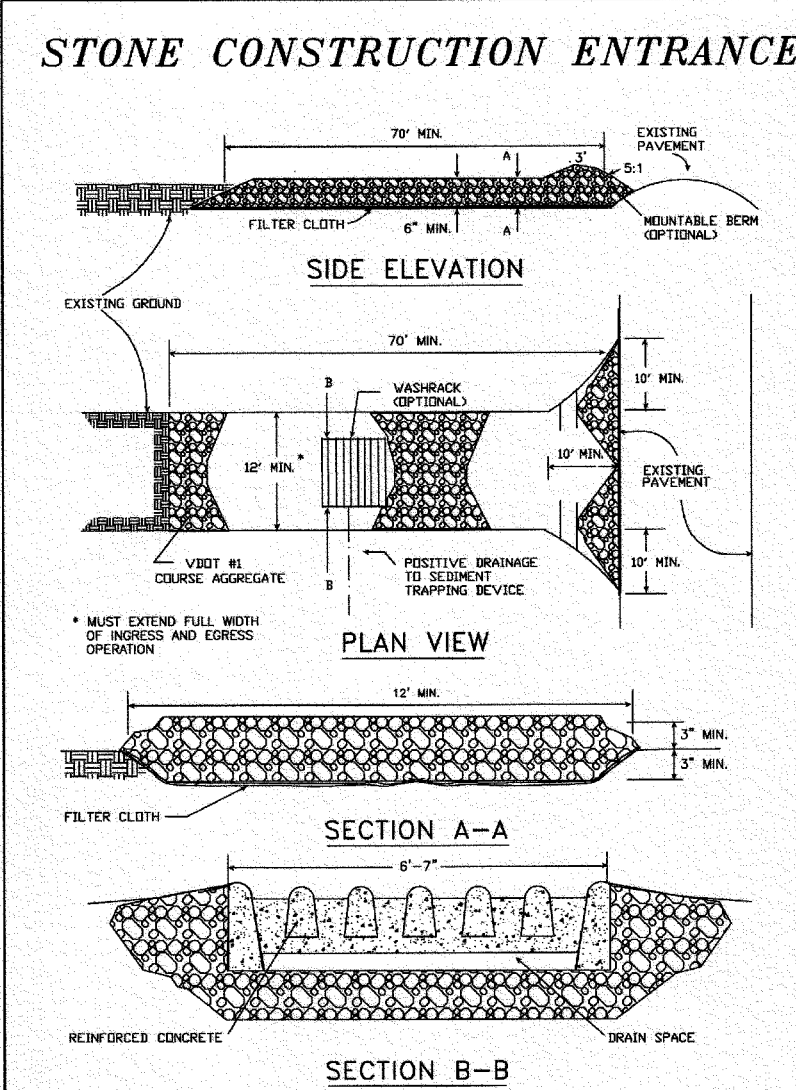
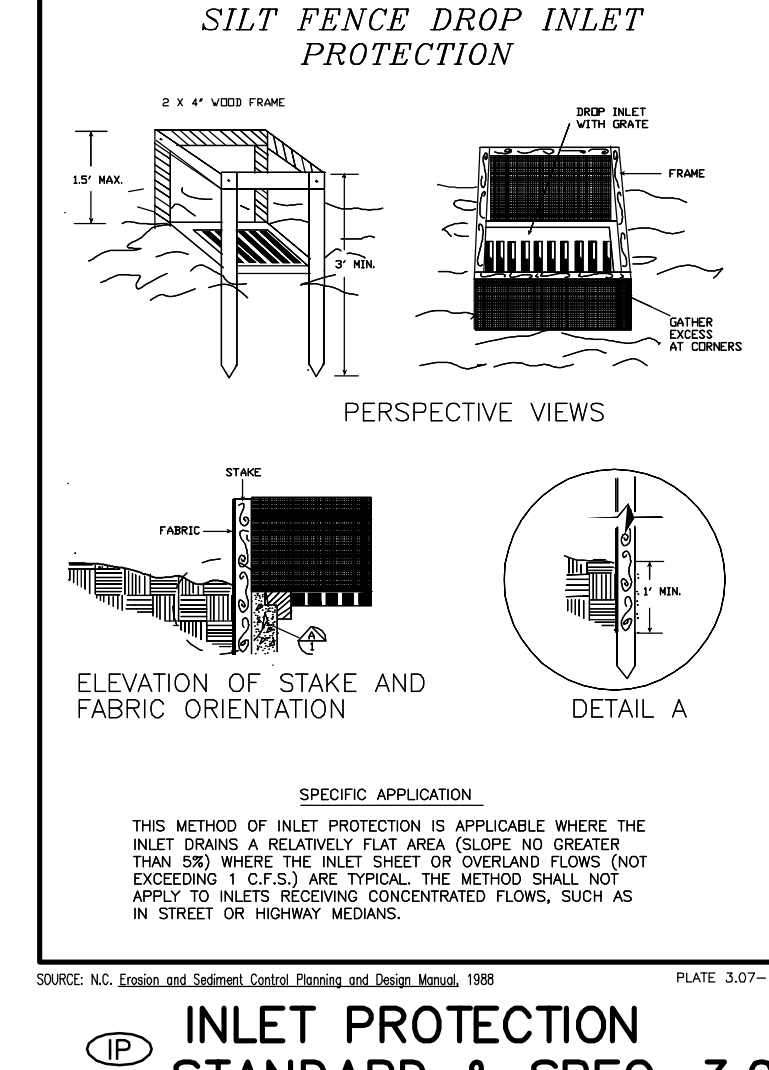
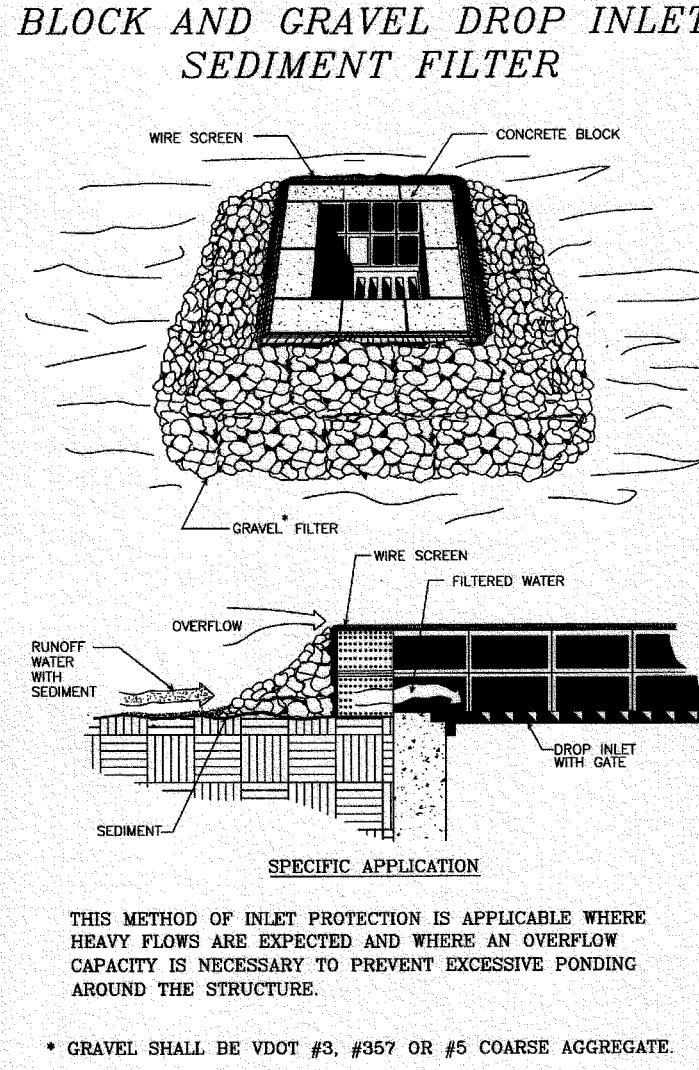
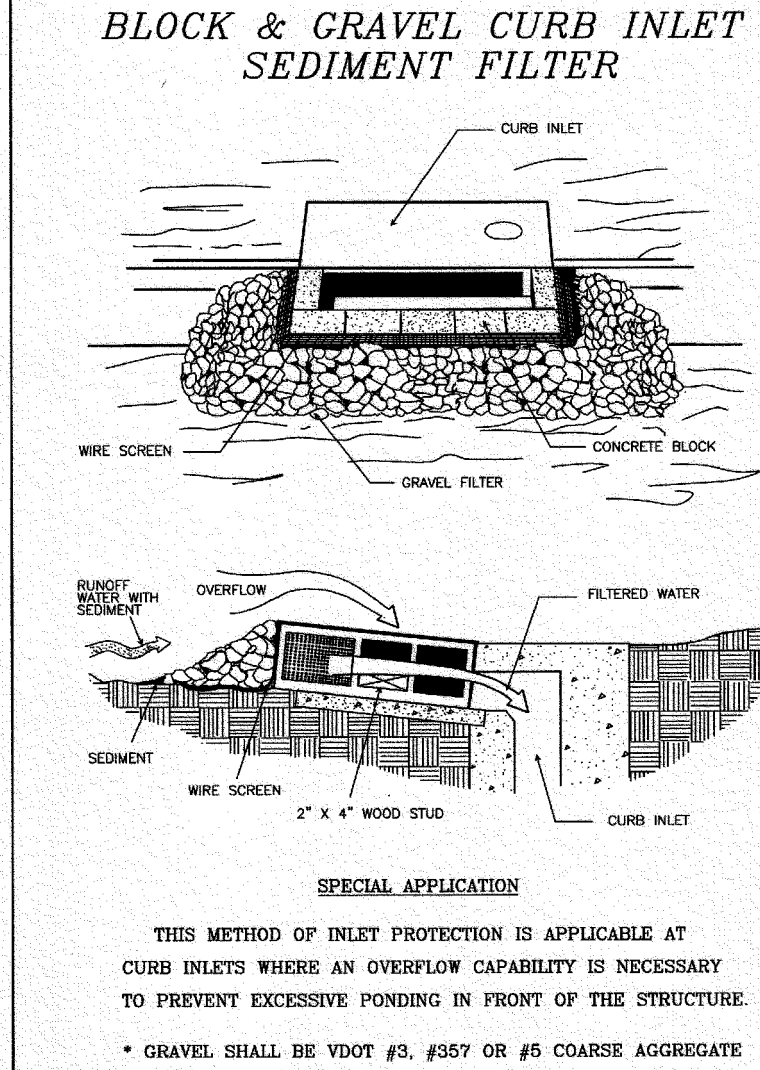
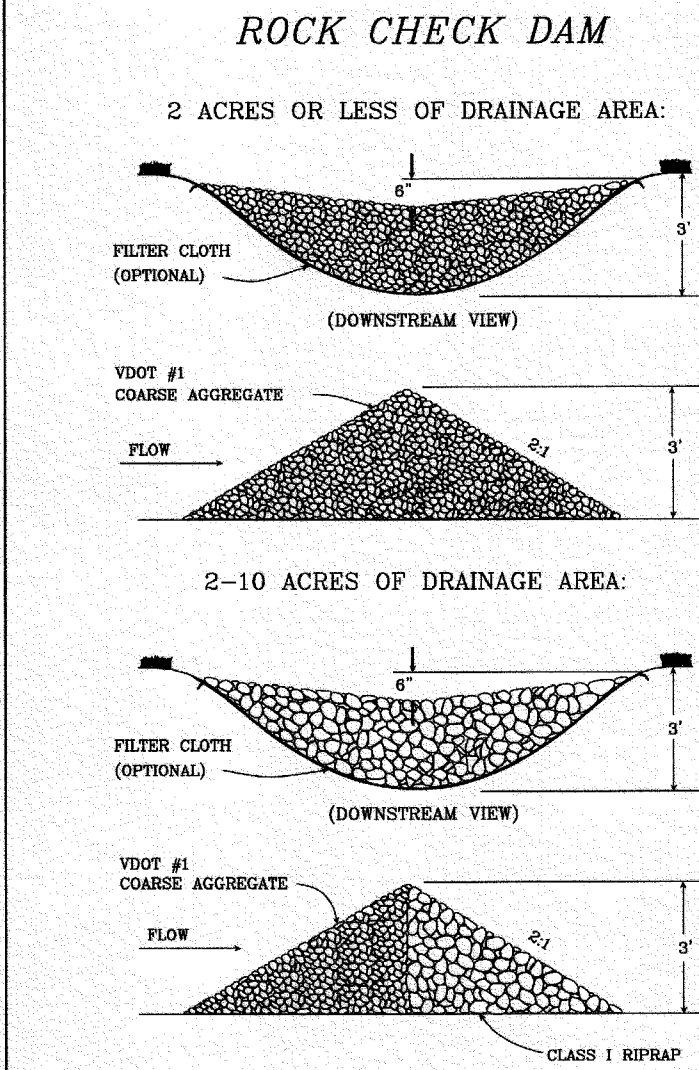


TABLE 3.32-E
(Revised June 2003)
PERMANENT SEEDING SPECIFICATIONS FOR COASTAL PLAIN AREA

SEED ¹		
LAND USE	SPECIES	APPLICATION RATES
<u>Minimum Care Lawn</u> (Commercial or Residential)	Tall Fescue ¹ or Bermudagrass ¹	175 - 200 lbs. 75 lbs.
	Tall Fescue ¹ or Bermudagrass ¹ (seed) or Bermudagrass ¹ (by other vegetative establishment method, see Std. & Spec. 3.34)	200-250 lbs. 40 lbs. (unhulled) 30 lbs. (hulled)
<u>High-Maintenance Lawn</u>	Tall Fescue ¹	128 lbs.
	Red Top Grass or Creeping Red Fescue	2 lbs.
	Seasonal Nurse Crop ²	20 lbs.
<u>General Slope (3:1 or less)</u>		TOTAL 150 lbs.
<u>Low-Maintenance Slope</u> (Steeper than 3:1)	Tall Fescue ¹	93-108 lbs.
	Bermudagrass ¹	0-15 lbs.
	Red Top Grass or Creeping Red Fescue	2 lbs.
	Seasonal Nurse Crop ²	20 lbs.
	Sericea Lespedeza ³	20 lbs.
		TOTAL: 150 lbs.

1 - When selecting varieties of turfgrass, use the Virginia Crop Improvement Association (VCIA) recommended turfgrass variety list. Quality seed will bear a label indicating that they are approved by VCIA. A current turfgrass variety list is available at the local County Extension office or through VCIA at 804-746-4884 or at <http://sudan.ces.vt.edu/html/Turf/turfpublications/publications2c.html>

2 - Use seasonal nurse crop in accordance with seeding dates as stated below:

February, March - April	Annual Rye
May 1 st - August	Foxtail Millet
September, October - November 15 th	Annual Rye
November 16 th - January	Winter Rye

3 - May through October, use hulled seed. All other seeding periods, use unhulled seed. If Weeping Lovegrass is used, include in any slope or low maintenance mixture during warmer seeding periods, increase to 30-40 lbs/acre.

- Apply 10-20-10 fertilizer at a rate of 500 lbs. / acre (or 12 lbs. / 1,000 sq. ft.)
- Apply Pulverized Agricultural Limestone at a rate of 2 tons/acre (or 90 lbs. / 1,000 sq. ft.)

- A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- Incorporate the lime and fertilizer into the top 4 – 6 inches of the soil by disk or by other means.
- When applying Slowly Available Nitrogen, use rates available in **Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites** at <http://www.dcr.state.va.us/sw/s&s.htm#pubs>

<u>SEED¹</u>		
LAND USE	SPECIES	APPLICATION PER ACRE
<u>Minimum Care Lawn</u> (Commercial or Residential)	Tall Fescue ¹	95-100%
	Perennial Ryegrass	0-5%
	Kentucky Bluegrass ¹	0-5%
		TOTAL: 175-200 lbs.
<u>High-Maintenance Lawn</u>	Tall Fescue ¹	TOTAL: 200-250 lbs.
<u>General Slope (3:1 or less)</u>	Tall Fescue ¹	128 lbs.
	Red Top Grass or Creeping Red Fescue	2 lbs.
	Seasonal Nurse Crop ²	20 lbs.
		TOTAL: 150 lbs.
<u>Low-Maintenance Slope</u> (Steeper than 3:1)	Tall Fescue ¹	108 lbs.
	Red Top Grass or Creeping Red Fescue	2 lbs.
	Seasonal Nurse Crop ²	20 lbs.
	Crownvetch ³	20 lbs.
		TOTAL: 150 lbs.

1 - When selecting varieties of turfgrass, use the Virginia Crop Improvement Association (VCIA) recommended turfgrass variety list. Quality seed will bear a label indicating that they are approved by VCIA. A current turfgrass variety list is available at the local County Extension office or through VCIA at 804-746-4884 or at <http://sudan.cses.vt.edu/html/Turf/turfpublications/publications2.html>

2 - Use seasonal nurse crop in accordance with seeding dates as stated below:

February 16 th - April	Annual Rye
May 1 st - August 15 th	Foxtail Millet
August 16 th - October	Annual Rye
November - February 15 th	Winter Rye

3 - Substitute *Sericea lopespedeza* for *Crownvetch* east of Farmville, VA (May through September use hulled seed, all other periods, use unhulled *Sericea*). If *Flatpea* is used, increase rate to 30 lbs./acre. If *Weeping Lovegrass* is used, include in any slope or low maintenance mixture during warm seeding periods, increase to 30-40

- Apply 10-20-10 **fertilizer** at a rate of **500 lbs. / acre** (or 12 lbs. / 1,000 sq. ft.)
- Apply **Pulverized Agricultural Limestone** at a rate of **2 tons/acre** (or 90 lbs. / 1,000 sq. ft.)


- A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- Incorporate the lime and fertilizer into the top 4 – 6 inches of the soil by disking or by other means.
- When applying Slowly Available Nitrogen, use rates available in [Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites](http://www.dcr.state.va.us/sw/e&s.htm#pubs) at <http://www.dcr.state.va.us/sw/e&s.htm#pubs>

SEED		
APPLICATION DATES	SPECIES	APPLICATION RATES
Sept. 1 - Feb. 15	50/50 Mix of Annual Ryegrass (lolium multi-florum) & Cereal (Winter) Rye (Secale cereale)	50 - 100 (lbs/acre)
Feb. 16 - Apr. 30	Annual Ryegrass (lolium multi-florum)	60 - 100 (lbs/acre)
May 1 - Aug. 31	German Millet	50 (lbs/acre)

- Apply 10-10-10 **fertilizer** at a rate of 450 lbs. / acre (or 10 lbs. / 1,000 sq. ft.)
- Apply **Pulverized Agricultural Limestone** at a rate of 2 tons/acre (or 90 lbs. / 1,000 sq. ft.)

- 1 - A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- 2 - Incorporate the lime and fertilizer into the top 4 – 6 inches of the soil by diskng or by other means.
- 3 - When applying Slowly Available Nitrogen, use rates available in **Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites** at <http://www.dcr.state.va.us/sw/e&s.htm#pubs>

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE:
 <p>CALLUP SURVEYORS & ENGINEERS, LTD. 523 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757) 428-8132 (757) 425-2390 FAX</p>		SCALE: NO SCALE	SHEET
		FILE NO.:	12/13
		C12	

EROSION AND SEDIMENT CONTROL NARRATIVE

EROSION AND SEDIMENT CONTROL NARRATIVE

PROJECT DESCRIPTION

THE PURPOSE OF THIS PROJECT IS THE EVENTUAL CONSTRUCTION OF A MULTI-PURPOSE TRANSLOADING FACILITY. THE OWNER WILL CONSTRUCT A SERIES OF BUILDINGS, SILOS, A RAILROAD SIDING, AND A WHARF TO LOAD AND OFFLOAD AGRICULTURAL COMMODITIES, SUCH AS GRAIN. THE SITE IS SERVED BY CITY WATER, A PUMP AND FORCEMAIN WILL BE USED TO CONVEY EFFLUENT TO AN EXISTING SANITARY FOREMAN. THE PURPOSE OF THIS PARTICULAR PLAN IS TO SHOW GRADING AND FILLING NECESSARY TO CONSTRUCT THE PROPOSED FACILITY. THE PROPOSED WHARF NECESSARY TO ACCOMMODATE SHIP AND BARGE TRAFFIC WILL BE PERMITTED UNDER A STANDARD JOINT PERMIT PLAN. A COMMERCIAL SITE PLAN WILL BE SUBMITTED IN THE FUTURE FOR THE TRANSLOADING FACILITY. THE POST DEVELOPED IMPERVIOUS AREA WILL BE GREATER THAN THE IMPERVIOUSNESS OF THE WATERSHED. THE DISTURBED AREA DURING CONSTRUCTION WILL BE 11.2 ACRES. THE SITE IS CURRENTLY DENuded AND PARTIALLY FILLED WITH GRAVEL AND CRUSHED CONCRETE.

EXISTING SITE CONDITIONS

THE PROPOSED SITE IS RELATIVELY FLAT (SLOPE < 1.5%) AND DRAINS TOWARDS THE RIVER MOST OF THE SITE CONSISTS OF A MIXTURE OF GRAVEL AND CRUSHED CONCRETE.

ADJACENT PROPERTY

ADJACENT PROPERTIES ARE INDUSTRIAL AND A NAVAL SHIPYARD. THE NORFOLK NAVAL SHIPYARD IS LOCATED ALONG THE NORTHERN BOUNDARY. THE SOUTHERN BRANCH OF THE ELIZABETH RIVER FORMS THE EASTERN BOUNDARY OF THE SITE AND ELM AVENUE IS LOCATED ALONG THE SOUTHERN END OF THE SITE. RECONSTRUCTION OF THE JORDAN BRIDGE, LOCATED ON ELM AVENUE, BEGAN THIS YEAR AND AS A RESULT, ELM AVENUE IN THIS AREA IS CLOSED. CONSTRUCTION OF THE PER SITE, AND THE ATLANTIC WOOD INDUSTRIES SUPERFUND PROJECT WILL OCCUR SIMULTANEOUSLY.

OFF-SITE AREAS

MINOR WORK IS PROPOSED IN THE RIGHT OF WAYS TO INCLUDE UTILITY HOOKUPS. NO STREET CONSTRUCTION IS PROPOSED. ALL DEMOLISHED HARDSCAPE WILL BE HAULED TO AN APPROVED DUMP SITE. ALL CONCRETE EXISTING HAS BEEN CRUSHED AND SPREAD ONSITE.

SOILS

THE SOILS REPORT PERFORMED INDICATES A CLAYEY SAND, SILTY SAND, AND LOW PLASTICITY CLAY (MIXTURE) INDICATING A LOW TO AVERAGE ERODIBILITY. THE DEPTH TO THE LOCAL GROUNDWATER TABLE IS APPROXIMATELY 2- FEET TO 6.5- FEET BELOW THE GROUND SURFACE, WITH THE SEASONAL ADJUSTED HIGH WATER TABLE ELEVATION AT 2.0

CRITICAL EROSION AREAS

THE SITE HAS SLOPES RANGING FROM 0 TO 1.5 PERCENT INDICATING A LOW EROSION HAZARD ON THE HIGH GROUND, AND 10% SLOPES ALONG THE SHORE, INDICATING A HIGH POTENTIAL FOR EROSION. THE PROPOSED WHARF WILL STOP THE EROSION.

EROSION AND SEDIMENT CONTROL MEASURES

UNLESS OTHERWISE INDICATED, ALL VEGETATIVE AND STRUCTURAL EROSION AND SEDIMENT CONTROL PRACTICES SHALL BE CONSTRUCTED AND MAINTAINED ACCORDING TO MINIMUM STANDARDS AND SPECIFICATIONS OF THE HANDBOOK. THE MINIMUM STANDARDS OF THE VESCR SHALL BE ADHERED TO UNLESS OTHERWISE WAIVED OR APPROVED BY A VARIANCE. WAIVERS MAY BE APPROVED ONLY THROUGH WRITTEN VARIANCE REQUESTS APPROVED BY THE CITY OF PORTSMOUTH.

STRUCTURAL PRACTICES

SILT FENCE BARRIER – 3.05

SILT FENCE BARRIERS WILL BE INSTALLED DOWN SLOPE OF AREAS WITH MINIMAL GRADES TO FILTER SEDIMENT-LADEN RUNOFF FROM SHEET FLOW AS INDICATED ON THE PLAN. SILT FENCE BARRIERS WILL ALSO BE PLACED AROUND THE PERIMETER NEAR THE PROPERTY LINE AND AROUND THE STOCKPILE.

TEMPORARY CONSTRUCTION ENTRANCE – 3.02

TWO 12' X 80' AND ONE 12' X 62' GRAVEL CONSTRUCTION ENTRANCES WILL BE USED FOR CONSTRUCTION ACCESS AS SHOWN ON THIS PLAN. DURING MUDDY CONDITIONS, DRIVERS OF CONSTRUCTION VEHICLES WILL BE REQUIRED TO WASH THEIR WHEELS BEFORE ENTERING THE ROADWAY. A STANDARD STONE CONSTRUCTION ENTRANCE IS SPECIFIED ON THIS PLAN.

MANAGEMENT STRATEGIES

- CONSTRUCTION WILL BE SEQUENCED SO THAT GRADING OPERATIONS CAN BEGIN AND END AS QUICKLY AS POSSIBLE.
- THE SITE IS BEING FILLED WITH GRAVEL AND CRUSHED CONCRETE. SEED AND MULCH IS NOT REQUIRED. INSTALLATION.
- THE JOB SUPERINTENDENT SHALL BE RESPONSIBLE FOR THE INSTALLATION AND MAINTENANCE OF ALL EROSION AND SEDIMENT CONTROL PRACTICES.
- AFTER ACHIEVING FULL DEVELOPMENT, THE TEMPORARY E&S CONTROLS WILL BE CLEANED UP AND REMOVED.
- STOCKPILES OF SOIL SHALL RECEIVE TEMPORARY SEEDING.

PERMANENT STABILIZATION

FILL SLOPES WILL BE STABILIZED WITH GRAVEL AND/OR RIP RAP.

STORMWATER RUNOFF CONSIDERATIONS

THE SITE WILL UTILIZE PERFORATED PIPE SURROUNDED BY GRAVEL AND WILL ALLOW FOR INFILTRATION PROVIDING BOTH WATER QUALITY AND QUANTITY CONTROL.

MAINTENANCE

IN GENERAL, ALL EROSION AND SEDIMENT CONTROL MEASURES WILL BE CHECKED DAILY AFTER EACH SIGNIFICANT RAINFALL. THE FOLLOWING ITEMS WILL BE CHECKED IN PARTICULAR:

- THE SILT FENCE BARRIER WILL BE CHECKED REGULARLY FOR UNDERMINING OR DETERIORATION OF THE FABRIC. SEDIMENT SHALL BE REMOVED WHEN THE LEVEL OF SEDIMENT DEPOSITION REACHES HALF WAY TO THE TOP OF THE BARRIER.
- EROSION CONTROLS WILL BE CHECKED REGULARLY AND ACCUMULATED SEDIMENT SHALL BE REMOVED AS NEEDED TO ENSURE THE PROPER FUNCTION OF THE DEVICES.
- INLET PROTECTION WILL BE CHECKED REGULARLY FOR SEDIMENT BUILDUP WHICH WILL PREVENT DRAINAGE. IF THE INLETS ARE CLOGGED BY SEDIMENT, THEY SHALL BE CLEANED OF SEDIMENT AND DEBRIS AND THE SEDIMENTS AND DEBRIS WILL BE HAULED TO AN APPROVED DUMP SITE.
- THE DEVELOPER SHALL MAINTAIN THE STONE CONSTRUCTION ENTRANCES BY RE-DRESSING OR REPLACING THE STONE, AS NECESSARY, TO PREVENT TRACKING OF SEDIMENTS ONTO PAVED AREAS.

CALCULATIONS

PRE AND POST DEVELOPED 10-YEAR STORM RUNOFF CALCULATIONS HAVE BEEN PERFORMED AS WELL AS WATER QUALITY CALCULATIONS. SEE "STORMWATER RUNOFF CONSIDERATIONS" ABOVE.

MITIGATION

2,721 SQ. FT. OF VEGETATED WETLANDS LOCATED AT THE SOUTHWEST CORNER OF THE SITE WILL BE FILLED BY THE EPA WITH THE PROJECT KNOWN AS "EAST SIDE CONTAINMENT FROM ATLANTIC WOOD INDUSTRIES SUPERFUND SITE." A CASH IN LIEU OF AGREEMENT IS BEING WORKED OUT BY THE DEVELOPER AND THE STATE.

DCR PLAN REVIEW MINIMUM STANDARD CHECKLIST

YES NO NA

[X] [] [] MS-1 Have temporary and permanent stabilization been addressed in narrative? Are practices shown on the plan?

[X] [] [] Seed specifications? Mulching? Gravel?

(Permanent or temporary soil stabilization shall be applied to denuded areas within seven days after final grade is reached on any portion of the site. Temporary soil stabilization shall be applied within seven days to denuded areas that may not be at final grade but will remain dormant for longer than 30 days. Permanent stabilization shall be applied to areas that are to be left dormant for more than one year.)

[X] [] [] MS-2 Has stabilization of soil stockpiles been addressed in narrative? Are sediment trapping measures provided?

(During construction of the project, soil stock piles and borrow areas shall be stabilized or protected with sediment trapping measures. The applicant is responsible for the temporary protection and permanent stabilization of all soil stockpiles on site as well as borrow areas and soil intentionally transported from the project site.)

[X] [] [] MS-3 Has maintenance of permanent stabilization been addressed?

(A permanent vegetative cover shall be established on denuded areas not otherwise permanently stabilized. Permanent vegetation shall not be considered established until a ground cover is achieved that is uniform, mature enough to survive and will inhibit erosion.)

[] [] [X] MS-4 Are sediment-trapping facilities to be constructed as a first step in LDA? Has maintenance of practices been addressed? (i.e. repair of structures and removal of accumulated sediment)

(Sediment basins and traps, perimeter dikes, sediment barriers and other measures intended to trap sediment shall be constructed as a first step in any land-disturbing activity and shall be made functional before upslope land disturbance takes place.)

[] [] [X] MS-5 Has stabilization of earthen structures been addressed?

(Stabilization measures shall be applied to earthen structures such as dams, dikes and diversions immediately after installation.)

[] [] [X] MS-6 Are sediment basins required where needed?

(Sediment traps and sediment basins shall be designed and constructed based upon the total drainage area to be served by the trap or basin.
a. The minimum storage capacity of a sediment trap shall be 134 cubic yards per acre of drainage area and the trap shall only control drainage areas less than three acres.
b. Surface runoff from disturbed areas that is comprised of flow from drainage areas greater than or equal to three acres shall be controlled by a sediment basin. The minimum storage capacity of sediment basin shall be 134 cubic yards per acre of drainage area. The outfall system shall, at minimum, maintain the structural integrity of the basin during a 25-year storm of 24-hour duration. Runoff coefficients used in runoff calculations shall correspond to a bare earth condition or those conditions expected to exist while the sediment basin is utilized.)

[X] [] [] MS-7 Has stabilization of cut and fill slopes been adequately addressed?

(Cut and fill slopes shall be designed and constructed in a manner that will minimize erosion. Slopes that are found to be eroding excessively within one year of permanent stabilization shall be provided with additional slope stabilizing measures until the problem is corrected.)

[] [] [X] MS-8 Are paved flumes, channels, or slope drains required where necessary?

(Concentrated runoff shall not flow down cut or fill slopes unless contained within an adequate temporary or permanent channel, flume or slope drain structure.)

[] [] [X] MS-9 Have water seeps from slope face, adequate drainage or other protection addressed?

(Whenever water seeps from a slope face, adequate drainage or other protection shall be provided.)

[X] [] [] MS-10 Is adequate inlet protection required on all operational storm sewer inlets?

(All storm sewer inlets that are made operable during construction shall be protected so that sediment-laden water cannot enter the conveyance system without first being filtered or otherwise treated to remove sediment.)

[X] [] [] MS-11 Are channel lining and/or outlet protection required on stormwater conveyance channels?

(Before newly constructed stormwater conveyance channels or pipes are made operational, adequate outlet protection and any required temporary or permanent channel lining shall be installed in both the conveyance channel and receiving channel.)

[X] [] [] MS-12 Are in-stream construction measures required so that channel damage is minimized?

(When work in a live watercourse is performed, precautions shall be taken to minimize encroachment, control sediment transport and stabilize the work area to the greatest extent possible during construction. Nonerodible material shall be used for the construction of causeways and cofferdams. Earthen fill may be used for these structures if armored by nonerodible cover materials.)

[] [] [X] MS-13 Are temporary stream crossings of non-erodible material required where necessary?

(When a live watercourse must be crossed by construction vehicles more than twice in any sixmonth period, a temporary vehicular stream crossing constructed of nonerodible material shall be provided.)

[] [] [X] MS-14 Are all applicable federal, state and local regulations pertaining to working it or crossing live watercourses being met?

(All applicable federal, state and local chapters pertaining to working in or crossing live watercourses shall be met.)

[] [] [X] MS-15 Has re-stabilization of areas subject to in-stream construction been adequately addressed?

(The bed and banks of a watercourse shall be stabilized immediately after work in the watercourse is completed.)

[X] [] [] MS-16 Has stabilization of utility trenches been addressed?

(Underground utility lines shall be installed in accordance with the following standards in addition to other applicable criteria:
a. No more than 500 linear feet of trench may be opened at one time.
b. Excavated material shall be placed on the uphill side of trenches.
c. Effluent from dewatering operations shall be filtered or passed through an approved sediment-trapping device, or both, and discharged in a manner that does not adversely affect flowing streams or off-site property.
d. Material used for backfilling trenches shall be properly compacted in order to minimize erosion and promote stabilization.
e. Restabilization shall be accomplished in accordance with this chapter.
f. Applicable safety chapters shall be complied with.)

YES NO NA

[X] [] [] MS-17 Has the prevention of transporting of soil and mud onto public roadways been adequately addressed? (i.e. Construction entrances, wash racks, daily cleaning of roadways, transport of sediment to a trapping facility.)

(Where construction vehicle access routes intersect paved or public roads provisions shall be made to minimize the transport of sediment by vehicular tracking onto the paved surface. Where sediment is transported onto a paved or public road surface, the road surface shall be cleaned thoroughly at the end of each day. Sediment shall be removed from the roads by shoveling or sweeping and transported to a sediment control disposal area. Street washing shall be allowed only after sediment is removed in this manner. This provision shall apply to individual development lots as well as to larger land-disturbing activities)

[X] [] [] MS- 18 Has the removal of temporary practices been addressed?

(All temporary erosion and sediment control measures shall all be removed within 30 days after final site stabilization or after the temporary measures are no longer needed unless otherwise authorized by the local program authority. Trapped sediment and the disturbed soil areas resulting from the disposition of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.)

[X] [] [] MS-19 Are properties and waterways downstream from the development adequately protected from erosion and sediment deposition due to increases in peak stormwater runoff?

(Properties and waterways downstream from development sites shall be protected from sediment deposition, erosion and damage due to increases in volume, velocity and peak flow rate of stormwater runoff for the stated frequency storm of 24-hour duration in accordance with the following standards and criteria:

- Concentrated stormwater runoff leaving a development site shall be discharged directly into an adequate natural or man-made receiving channel, pipe or storm sewer system. For those sites where runoff is discharged into a pipe or pipe system, downstream stability analyses at the outfall of the pipe or pipe system shall be performed.
- Adequacy of all channels and pipes shall be verified in the following manner:
 - The applicant shall demonstrate that the total drainage area to the point of analysis within the channel is one hundred times greater than the contributing drainage area of the project in question; or
 - (a) Natural channels shall be analyzed by the use of a two-year storm to verify that stormwater will not overtop channel banks nor cause erosion of channel bed or banks.
(b) All previously constructed man-made channels shall be analyzed by the use of a ten-year storm to verify that stormwater will not overtop its banks and by the use of a two-year storm to demonstrate that stormwater will not cause erosion of channel bed or banks; and
(c) Pipes and storm sewer systems shall be analyzed by the use of a ten-year storm to verify that stormwater will be contained within the pipe or system.
 - If existing natural receiving channels or previously constructed man-made channels or pipes are not adequate, the applicant shall:
 - Improve the channels to a condition where a ten-year storm will not overtop the banks and a two-year storm will not cause erosion to channel the bed or banks; or
 - Improve the pipe or pipe system to a condition where the ten-year storm is contained within the appurtenances;
 - Develop a site design that will not cause the pre-development peak runoff rate a two-year storm to increase when runoff outfalls into a natural channel or will not cause the pre-development peak runoff rate from a ten-year storm to increase when runoff outfalls into a man-made channel; or
 - Provide a combination of channel improvement, stormwater detention or other measures which is satisfactory to the plan approving authority to prevent downstream erosion.
 - The applicant shall provide evidence of permission to make the improvements.
 - All hydrologic analyses shall be based on the existing watershed characteristics and the ultimate development condition of the subject project.
 - If the applicant chooses an option that includes stormwater detention, he shall obtain approval from the locality of a plan for maintenance of the detention facilities. The plan shall set forth the maintenance requirements of the facility and the person responsible for performing the maintenance.
 - Outfall from a detention facility shall be discharged to a receiving channel, and energy dissipators shall be placed at the outfall of all detention facilities as necessary to provide a stabilized transition from the facility to the receiving channel.
 - All on-site channels must be verified to be adequate.
 - Increased volumes of sheet flows that may cause erosion or sedimentation on adjacent property shall be diverted to a stable outlet, adequate channel, pipe or pipe system, or to a detention facility.
 - In applying these stormwater management criteria, individual lots or parcels in a residential, commercial or industrial development shall not be considered to be separate development projects. Instead, the development, as a whole, shall be considered a single development project. Hydrologic parameters that reflect the ultimate development condition shall be used in all engineering calculations.
 - All measures used to protect properties and waterways shall be employed in a manner which minimizes impacts on the physical, chemical and biological integrity of rivers, streams and other waters of the state.

EROSION CONTROL NOTES

PORTSMOUTH TERMINAL FACILITY

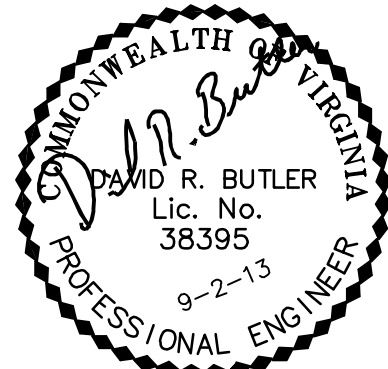
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA MADE FOR: PER PROPERTIES

DESIGN BY: BWG DRAWN BY: JB CHECKED BY: BWG DATE: OCTOBER 2, 2013

GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX

SCALE: NO SCALE SHEET 13/13

C13



DATE	COMMENT
REVISION SCHEDULE	